Large Generators and High Power Drives

Contents of lectures

Source:

Siemens AG, Germany

3. Eddy current losses in winding systems

3. Eddy current losses in winding systems

3.1 Additional losses in electrical machines

Losses in synchronous machines at sinusoidal line voltage operation

A) No-load losses: (I_s = 0):

A1) **Iron losses** (Eddy current & hysteresis losses) in stator iron teeth and yoke
A2) **Friction losses** (Bearings, brushes)
A3) **Ventilation (windage) losses** (Fan power, rotor surface friction)
A4) **Additional no-load losses**

B) Losses at load: (occur in addition to A), if I_s > 0):

B1) **Ohmic losses in stator winding**
B2) **Stray load losses (= additional losses at load)**

C) Excitation losses:

C1) **Ohmic losses in rotor field winding**
C2) **Electric losses in brushes**

C3) **Losses in exciter** (= exciting machine or power electronics)

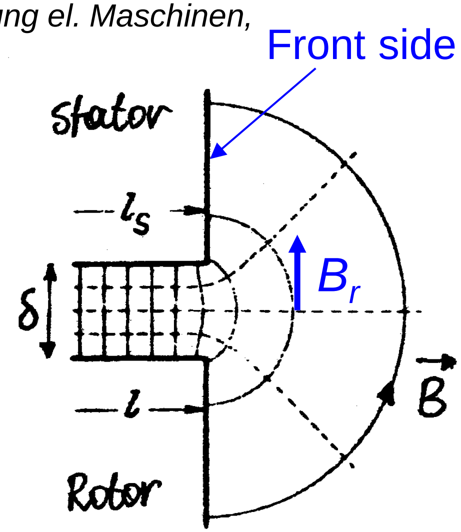
3. Eddy current losses in winding systems

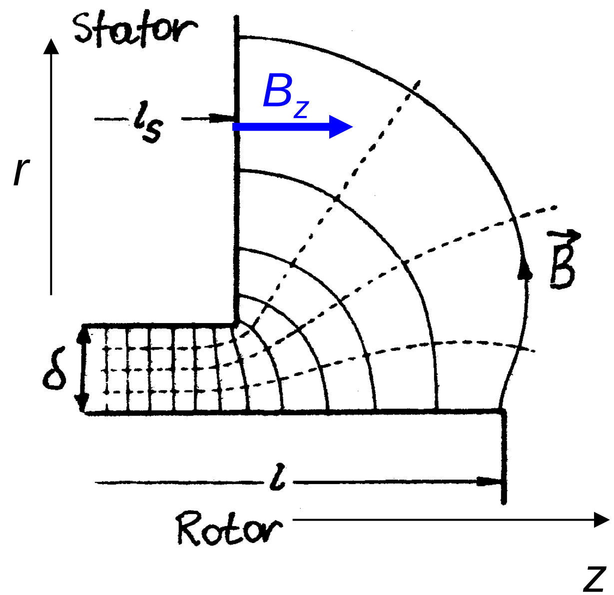
Additional no-load losses

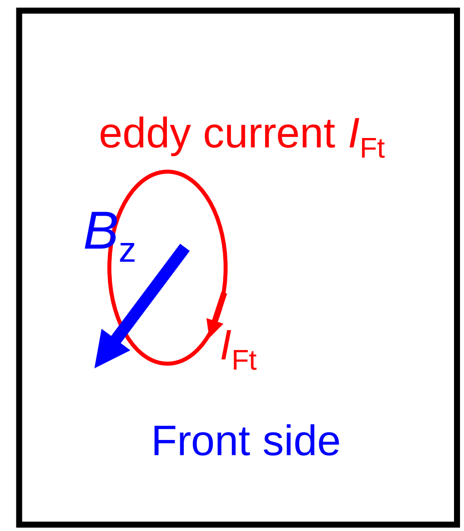
Axial component B_z of no-load end field

- **Main flux density in air gap has end field component, penetrating press plates axially**
- **Big machines: big press plates = big surface for axial flux = big eddy currents**

Source: Vogt, K.; Berechnung el. Maschinen, VEB

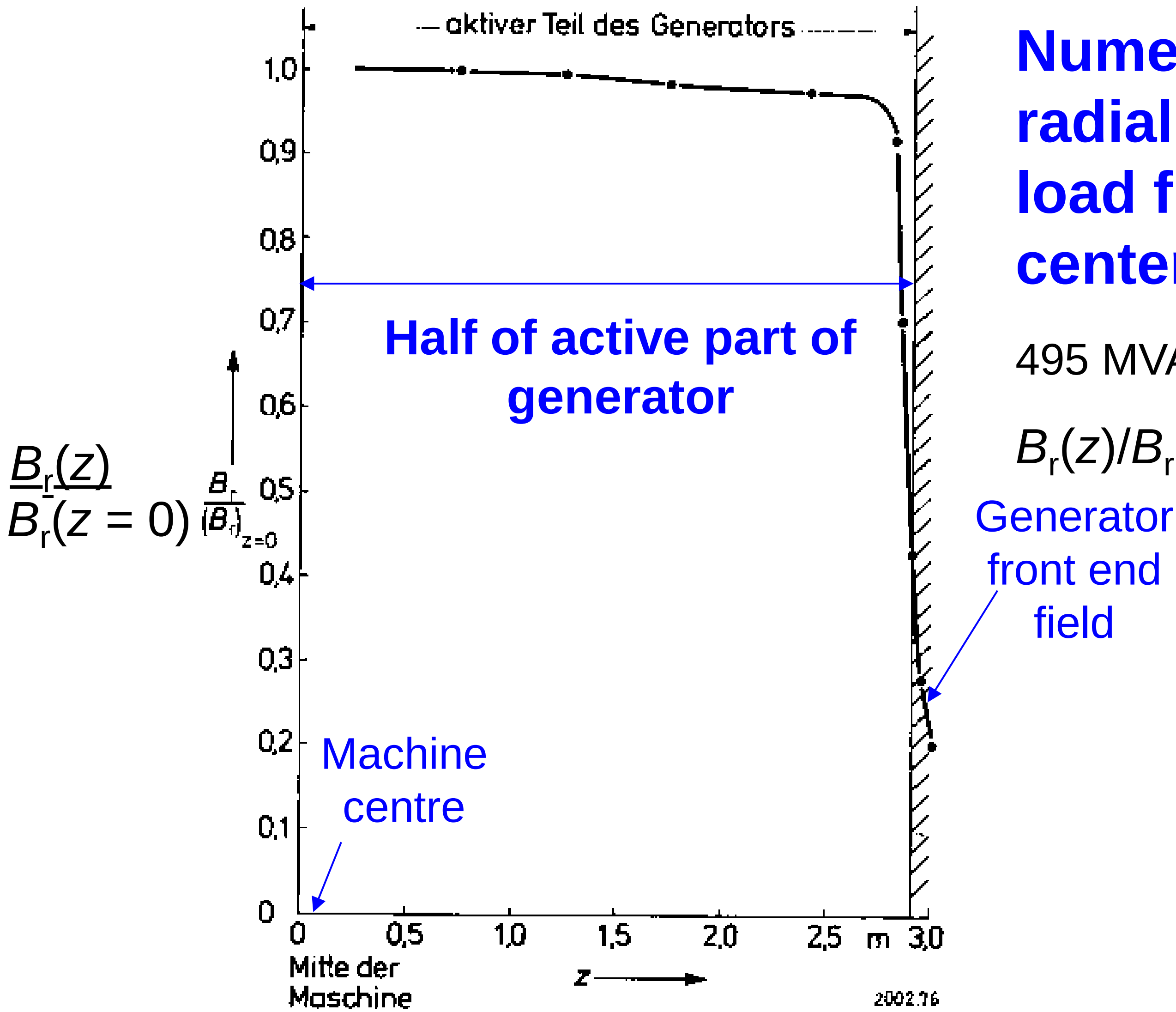






Axial flux-density component B_z penetrates iron sheets perpendicular, induces eddy currents in the end zone packets and the end press plates = additional no-load losses

3. Eddy current losses in winding systems



Numerically calculated radial component of the no-load flux density in the center of the air-gap

495 MVA, 2-pole turbine generator:

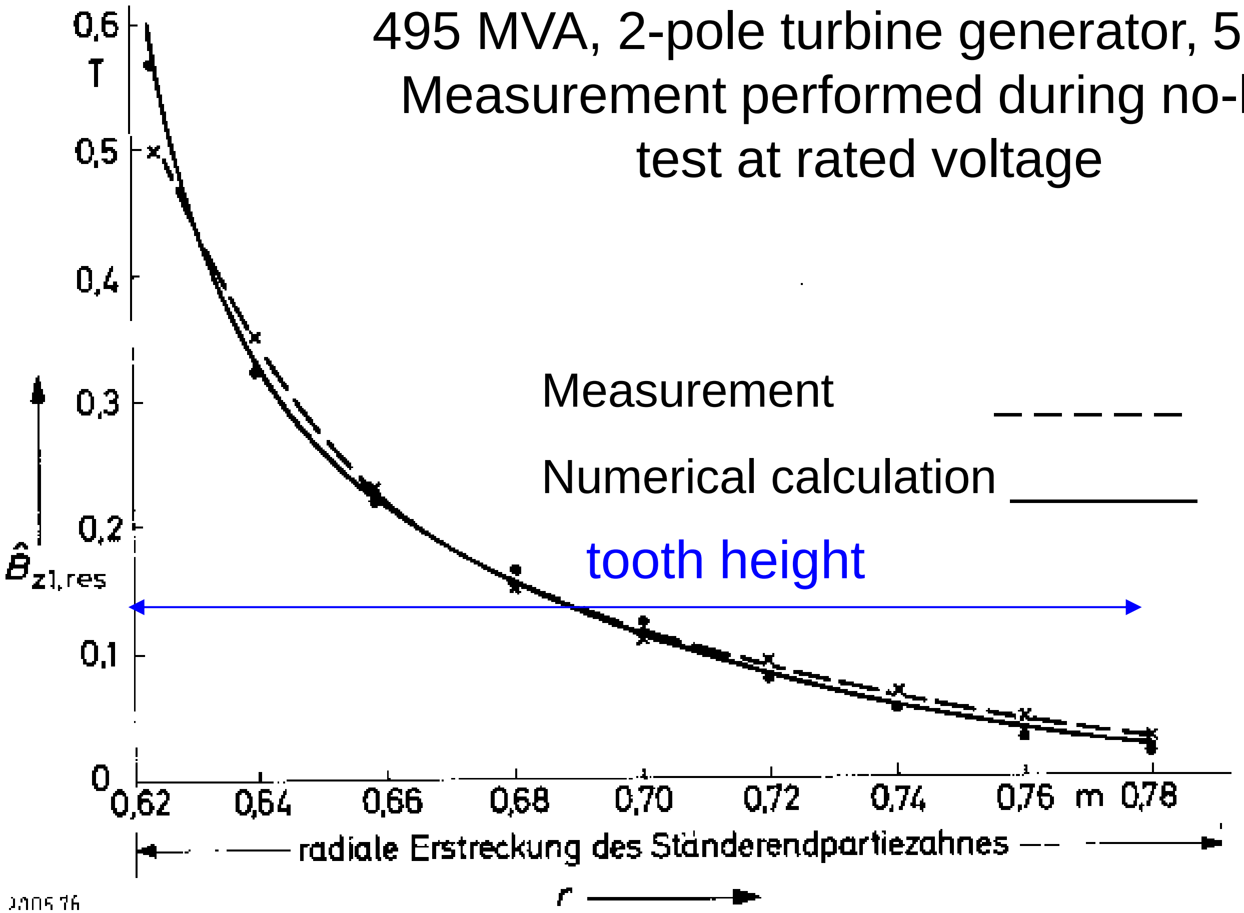
$B_r(z)/B_r(z = 0)$

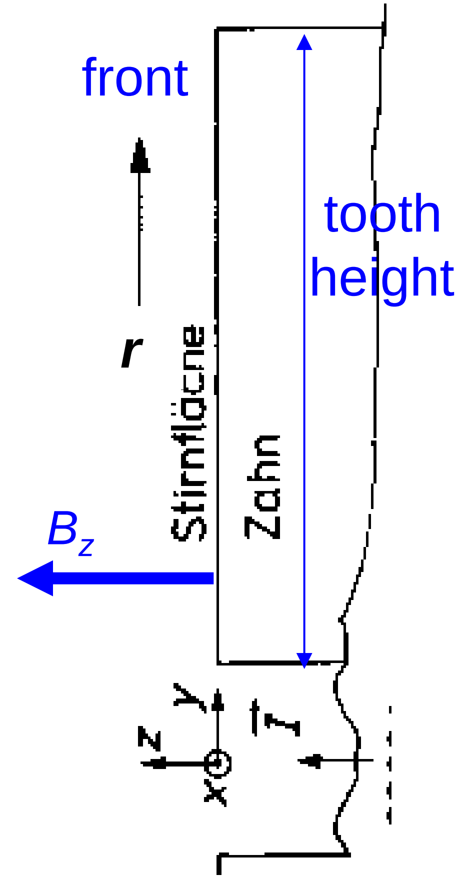
Source: AEG, Germany

3. Eddy current losses in winding systems

B_z (amplitude of fundamental no-load sine wave field) at the front end along the tooth height in radial direction

495 MVA, 2-pole turbine generator, 50 Hz:
Measurement performed during no-load test at rated voltage





Source: AEG, Germany

3. Eddy current losses in winding systems

Reduction of end-zone eddy current losses

- Partitioning of end plates reduces eddy current paths
- Slitting of press fingers reduces eddy current paths
- Non-magnetic press plates reduce the magnetic field B_z (e.g. aluminium, stainless steel)
- Stepping of end packet increases the end-zone air gap to reduce the field
- Laminated glued press plates
- Copper shielding of press plates: The eddy currents flow in the low-resistive copper-shield. Their self-field opposes the intruding field B_z, which does no enter the press-plate

3. Eddy current losses in winding systems

Losses in press plates and press fingers

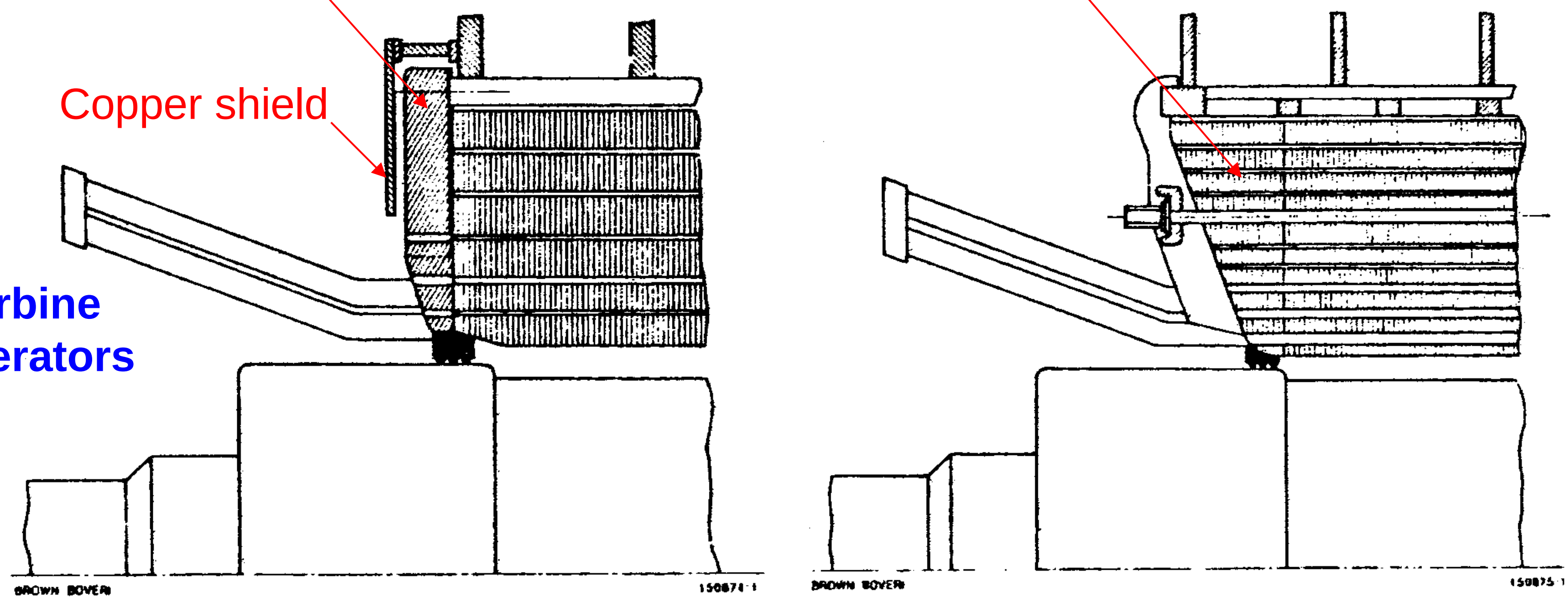
Axial end field component B_z induces with stator frequency eddy currents I_{Ft} in press plates

Aluminium press plate
(lower power range < 400 MW)

Laminated glued steel press plate
(high power range up to 2 GW)

Copper shield

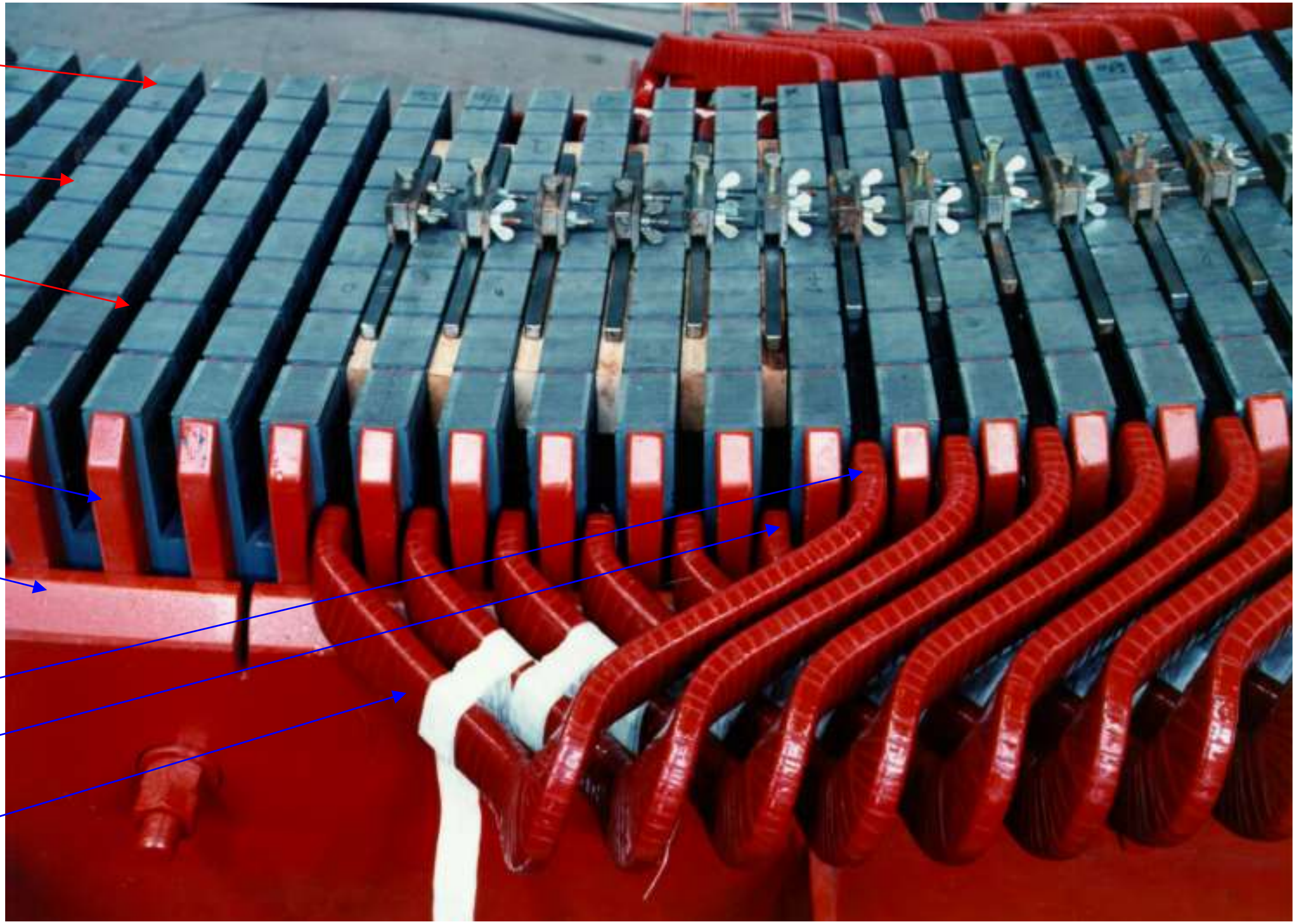
Turbine generators



Source: Neidhöfer, G.; BBC (now Alstom), Switzerland

3. Eddy current losses in winding systems

End zone of synchronous hydro generator with high pole count



Source:

VATech Hydro, (now Andritz Hydro) Austria

3. Eddy current losses in winding systems

Stepping of end packet to increase end-zone air-gap

Due to increased end-zone air-gap the end-zone flux density is reduced = lower end zone eddy current losses

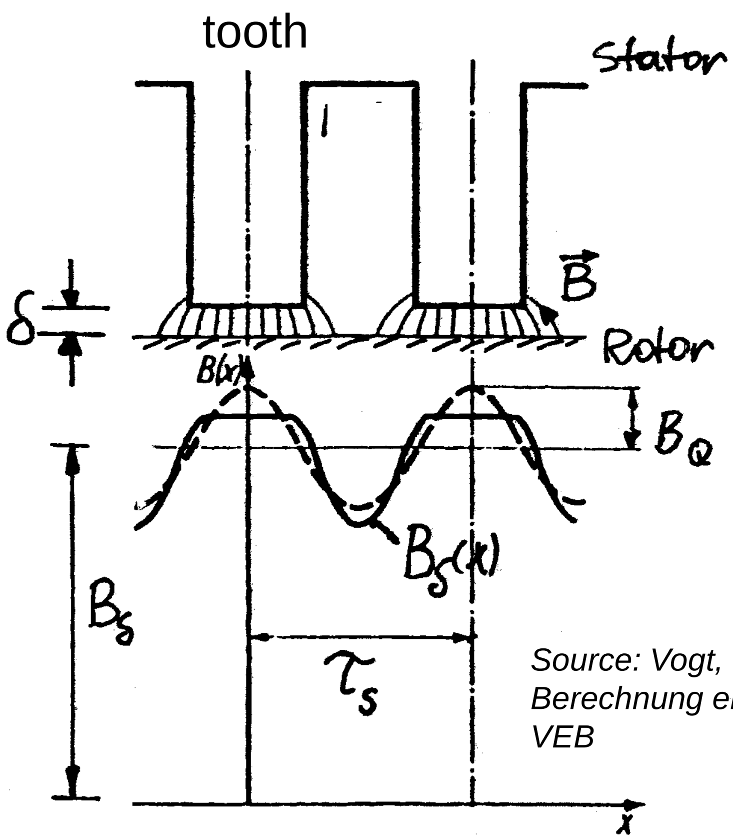
Source:

VATech Hydro, (now Andritz Hydro) Austria

3. Eddy current losses in winding systems

Rotor pole shoe losses at no-load

- High voltage winding demands open stator slots, which cause ripple in air gap magnetic flux density



Source: Vogt, K.; Berechnung el. Maschinen, VEB

- Slot-frequent ripple causes induced voltage in rotor pole shoe surface, hence eddy current losses occur !

- Frequency: $f_Q = n \cdot Q$

(in kHz-range !: e.g. 36 slots, 3000/min: f_Q = 1800 Hz)

- Reduction of pole shoe losses:

- Laminated pole shoes
- Magnetic stator slot wedges
- Grooving of rotor press plates

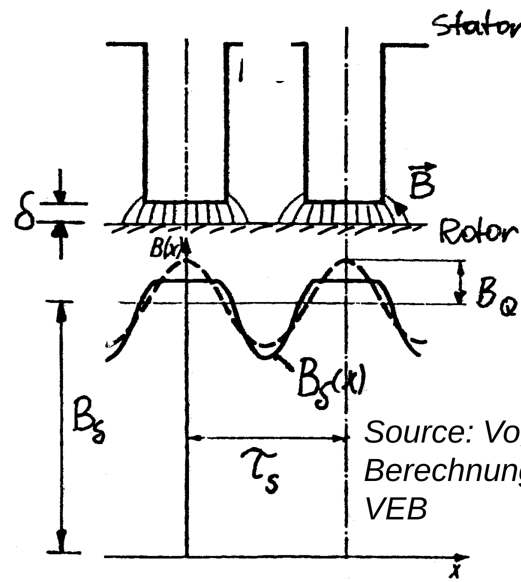
3. Eddy current losses in winding systems

Manufacturing of poles for high pole count low speed ring generator

Pole shoes, built as laminated iron stack to suppress eddy currents, which are induced by slot ripple magnetic air gap field due to stator slot openings

Also the damper is induced = losses

Slots for damper bars



Source: Vogt, K.; Berechnung el. Maschinen, VEB

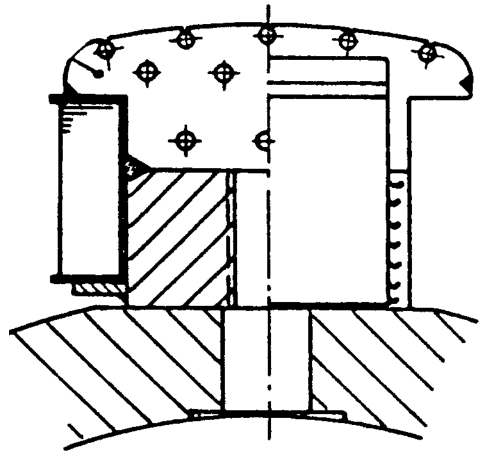
Source: Andritz Hydro, Austria

3. Eddy current losses in winding systems

Massive rotor pole shaft welded to laminated pole shoes

Laminated pole shoes

Massive pole shaft (welded)



Source: Gregori, F.; TU Wien

Source:

VATech Hydro,
(now Andritz Hydro) Austria

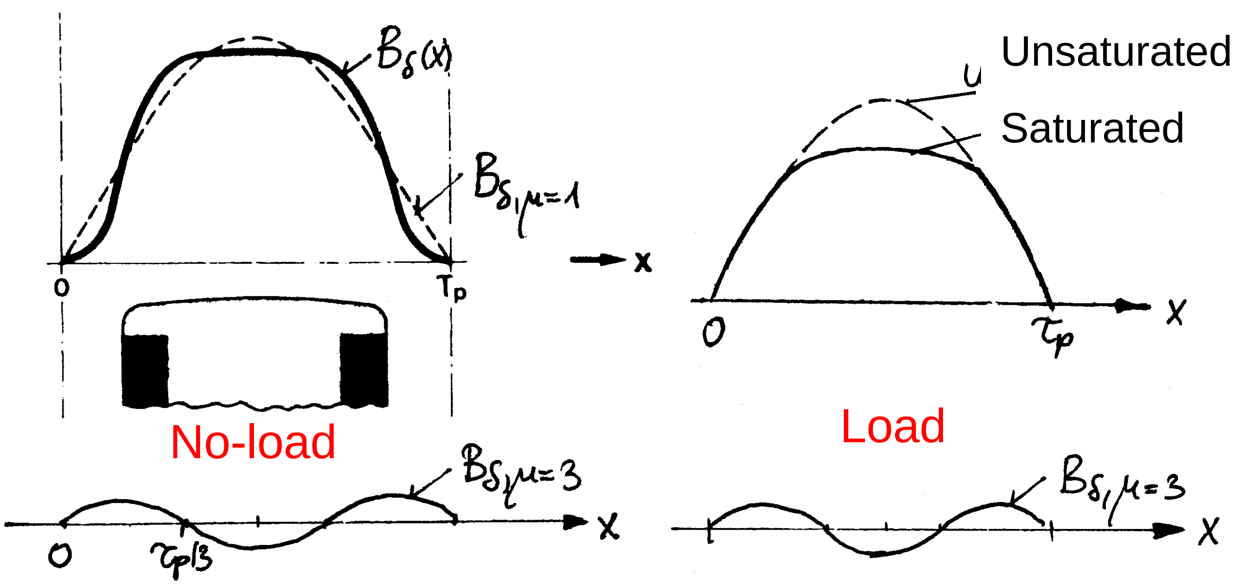
3. Eddy current losses in winding systems

Additional load losses

- **Stator iron losses due to 3rd harmonic of air gap field**

- Already at no-load 3rd harmonic due to shape of air gap exists in salient pole machines !

- At load stator and rotor field give increased flux: Saturation occurs, causing increased 3rd harmonic



- 3rd harmonic stator frequency is 3-times line frequency

e.g. 150 Hz

- Reduction of losses:

Optimization of air gap

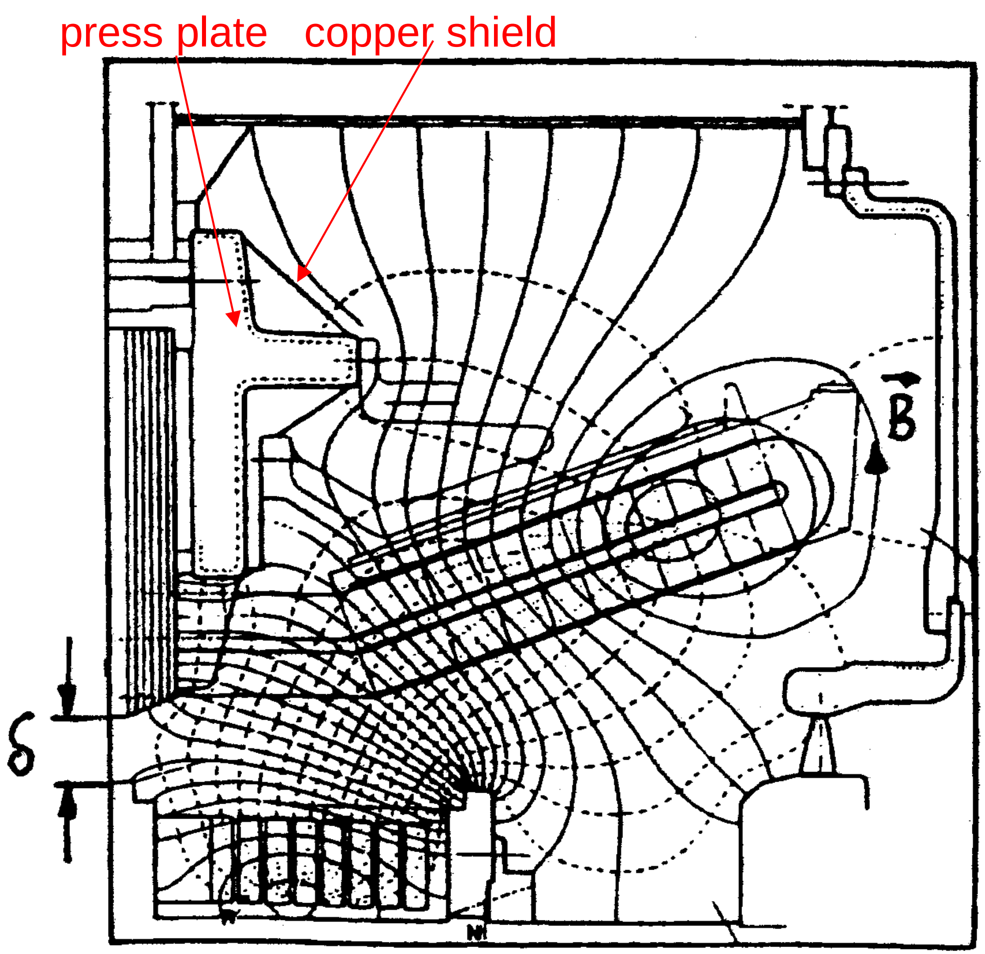
Low loss iron sheets

Source:

Bohn, T. (Ed.), TÜV Rheinland

3. Eddy current losses in winding systems

Increase of press plate end-zone losses under load



Source: Darrieux, G., ABB, Switzerland

- Winding overhang of stator and rotor winding excite stray field with line frequency

- Axial component causes considerable eddy current losses in press plates

- Reduction of losses:

- Partitioning of end plates,

- Slitting of press fingers,

- Non-magnetic press plates to reduce magnetic field (Aluminium, stainless steel),

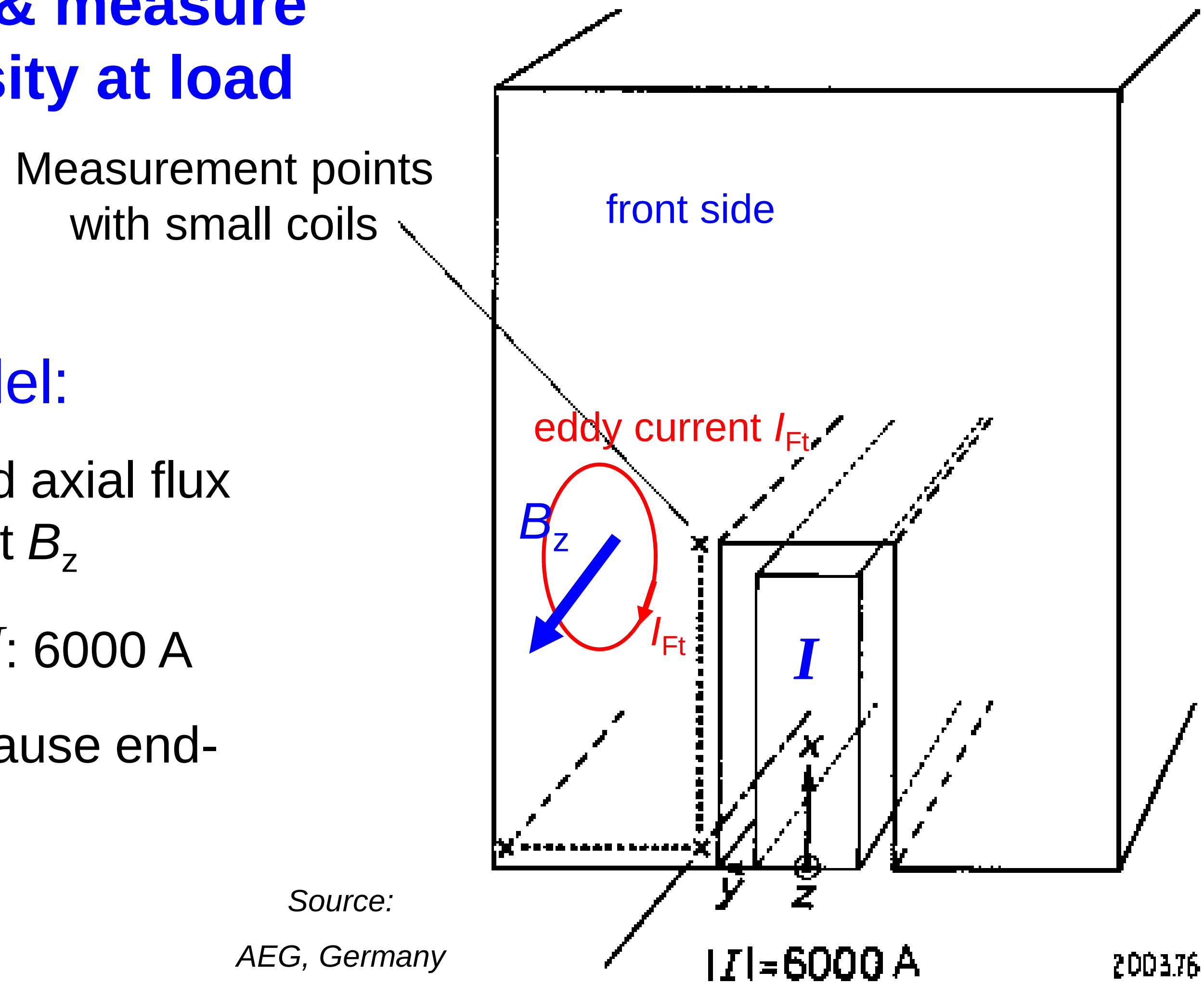
- Stepping of end packet (= increase of air gap) to reduce field,

- laminated glued press plates,

- Copper shielding

3. Eddy current losses in winding systems

Model to calculate & measure end zone flux density at load



Source:

AEG, Germany

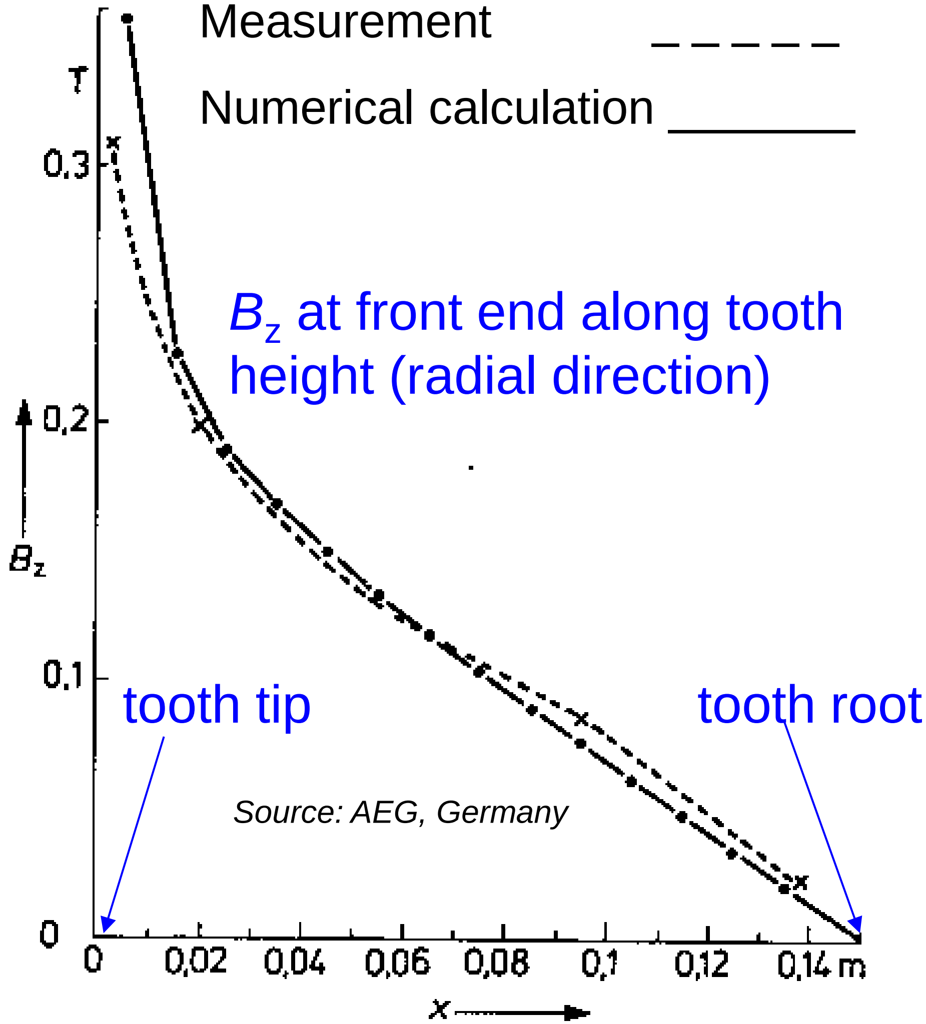
Stator slot model:

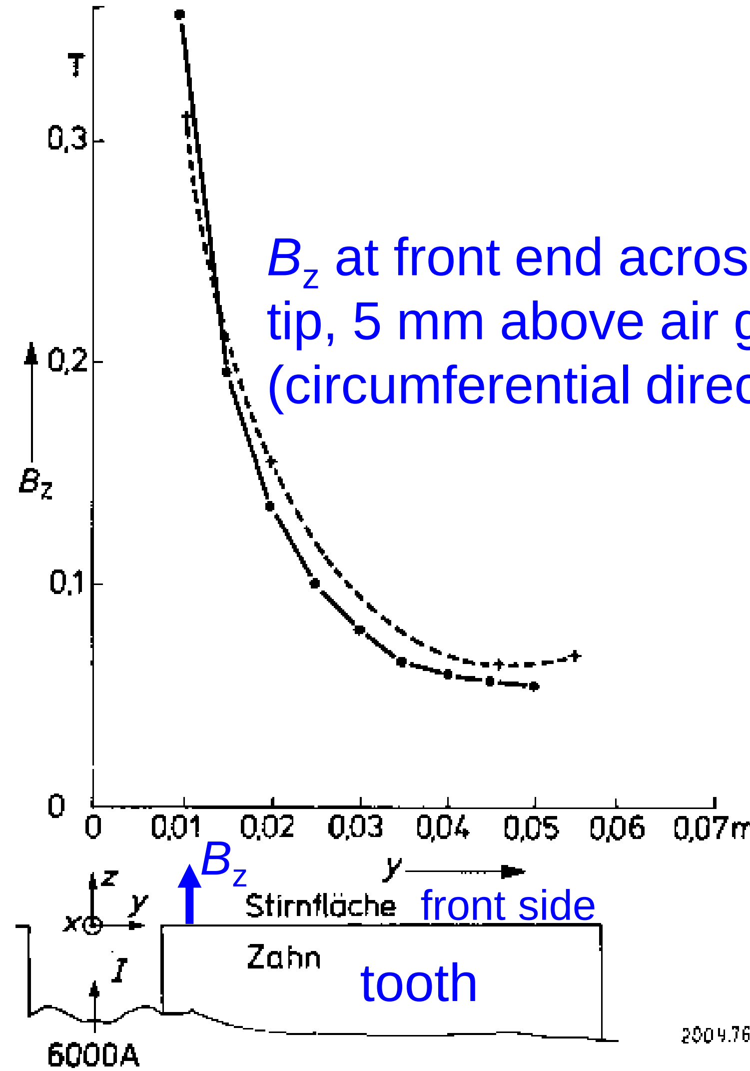
Measurement of front end axial flux density component B_z

Slot conductor current I: 6000 A

Induced eddy currents cause end-zone losses

3. Eddy current losses in winding systems

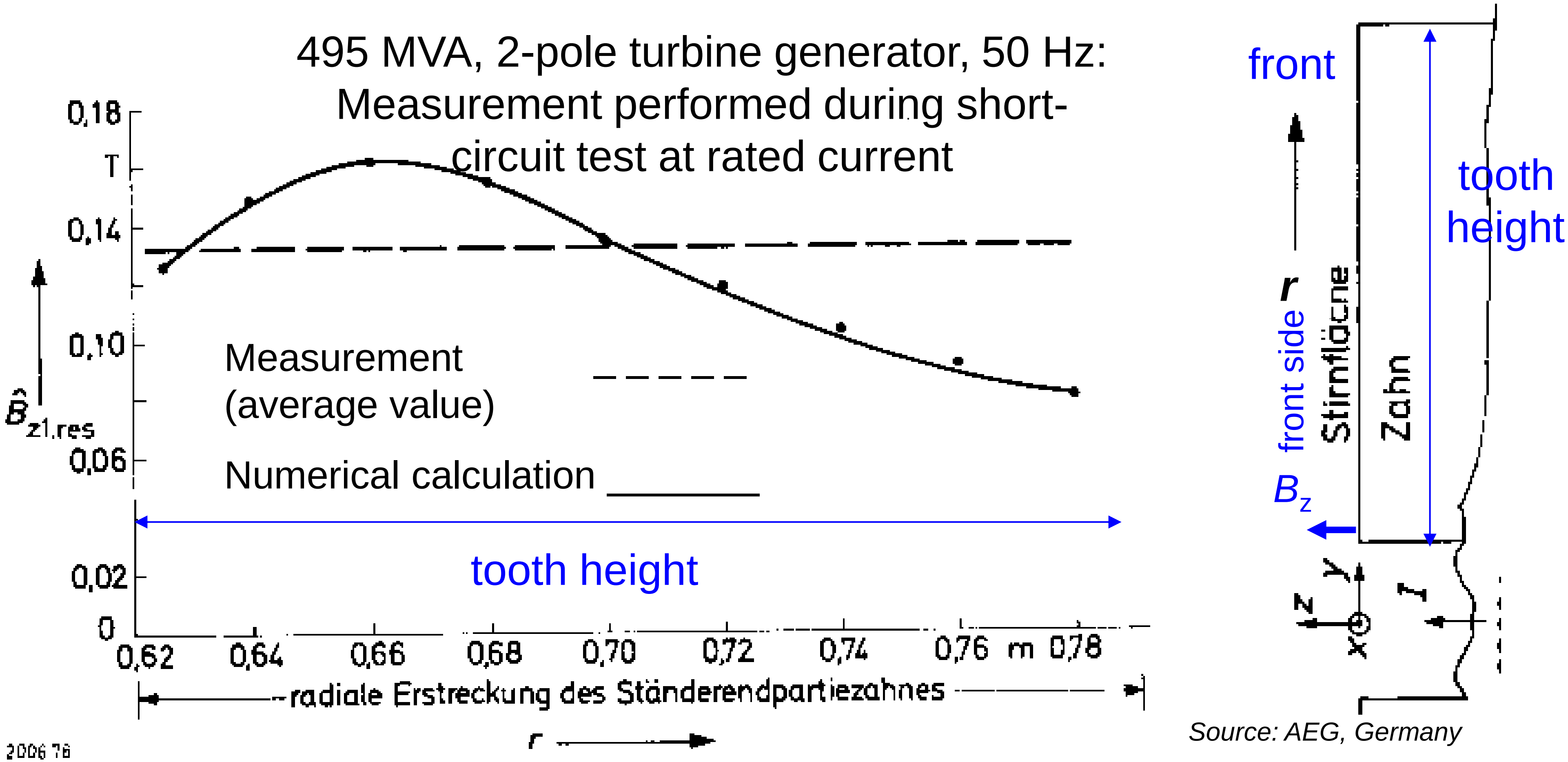




3. Eddy current losses in winding systems

B_z (amplitude of fundamental sine wave field) at <u>stator winding short-circuit</u> at the front end along the tooth height in radial direction

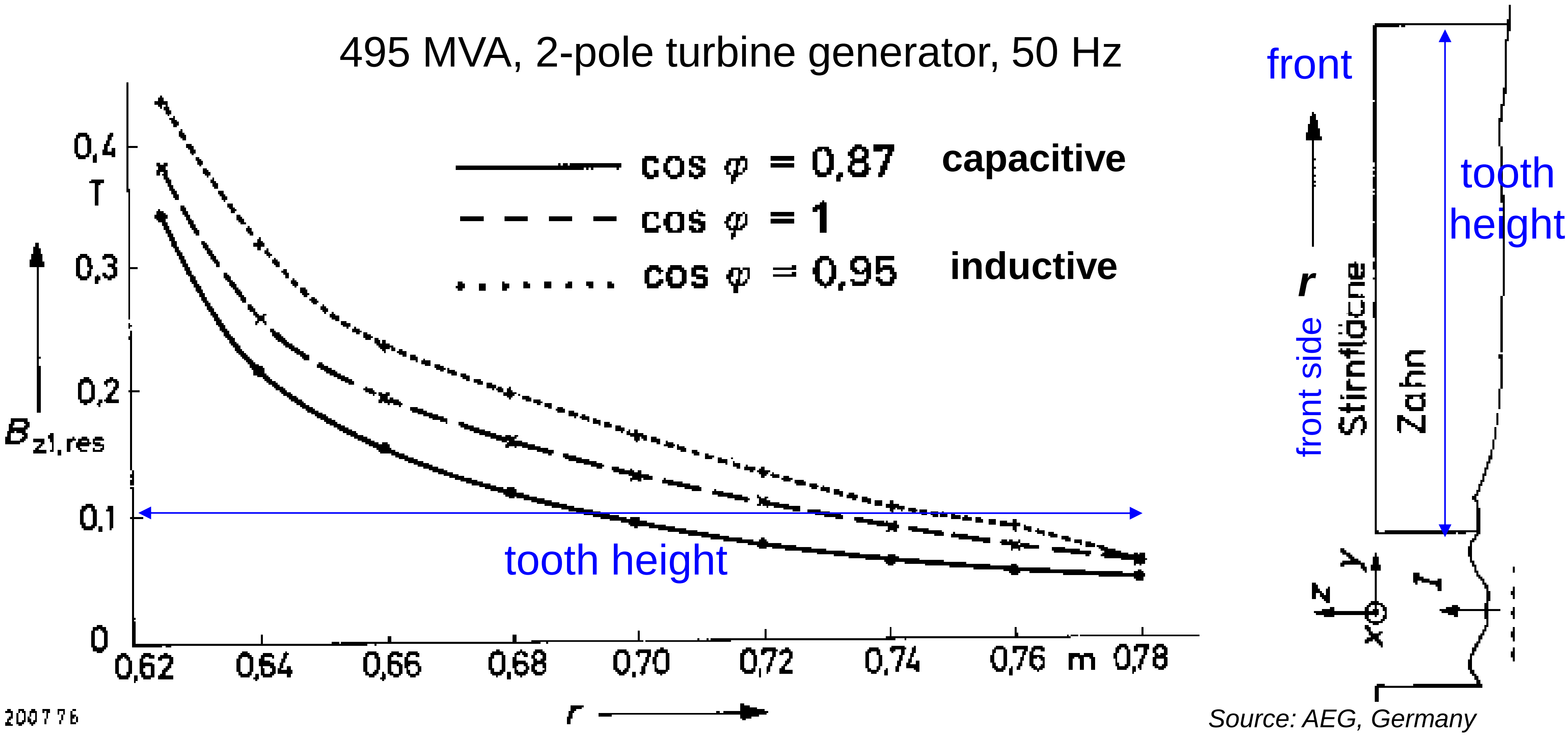
495 MVA, 2-pole turbine generator, 50 Hz:
Measurement performed during short-circuit test at rated current



Source: AEG, Germany

3. Eddy current losses in winding systems

Calculated amplitude of fundamental sine wave field B_z at rated stator voltage and current at the front end along the tooth height in radial direction



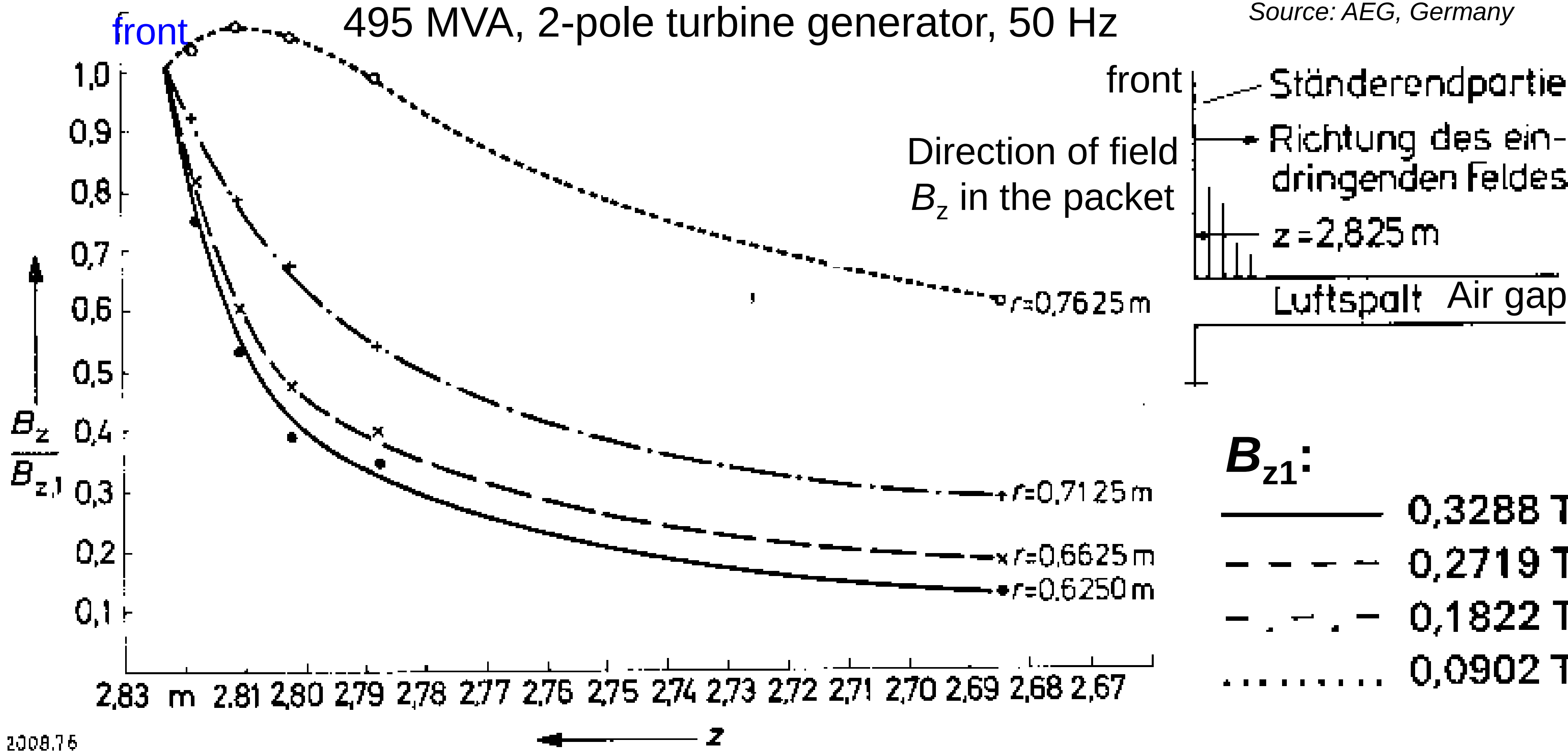
Source: AEG, Germany

3. Eddy current losses in winding systems

Calculated amplitude of fundamental sine wave field B_z at rated stator voltage and current in the first iron end packet in axial direction

495 MVA, 2-pole turbine generator, 50 Hz

Source: AEG, Germany



Summary:

Additional losses in electrical machines

- Additional no-load losses (stator current is zero) in the iron core, the rotor pole shoes & the damper cage and the end zones
- Additional losses at load due to current displacement in the stator winding, in the rotor pole shoes & damper cage due to stator space harmonic fields and in the end zone

3. Eddy current losses in winding systems

3.1 Additional losses in electrical machines

3.2 Basics on current displacement

3.3 Current displacement in massive slot conductor

3.4 Critical conductor height

3.5 Use of current displacement in electrical machines

3.6 Methods to reduce current displacement effect

3.7 Air-gap winding for superconducting machines

3. Eddy current losses in winding systems

3.2 Basics on current displacement

- Big generators: Big power leads to big current !

- Big current needs big conductor cross section, so conductor height is big !

- Usually in big generators number of turns per coil is N_c = 1: = BAR !

- Stator current causes slot stray flux, pulsating with line frequency, which induces eddy currents in conductor itself = additional load losses !

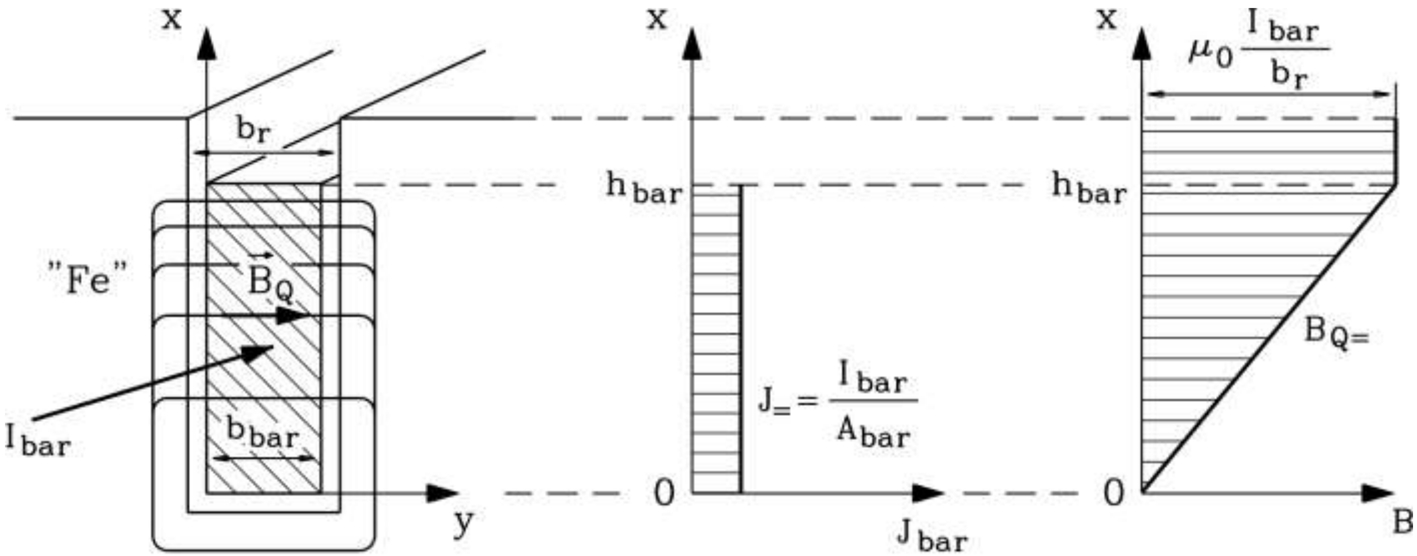
- Eddy currents are superimposed on bar current; they cause unequal current density distribution!

- Current flows to greater part in upper conductor half = current displacement !

3. Eddy current losses in winding systems

Slot conductor & slot stray flux at DC

- If current density $J_{bar} = I_{bar} / A_{bar}$ is homogeneously distributed over bar cross section, then slot stray field, which crosses slot perpendicular to slot axis, increases linear with bar height *x* !



- **AMPERE´s law:** $\oint_C \vec{H} \cdot d\vec{s} = H_Q(x) \cdot b_r = J \cdot x \cdot b_{bar}$

$$B_Q(x) = \mu_0 J \frac{x \cdot b_{bar}}{b_r} = \mu_0 \frac{I_{bar}}{b_r} \cdot \frac{x}{h_{bar}}, 0 \le x \le h_{bar}$$

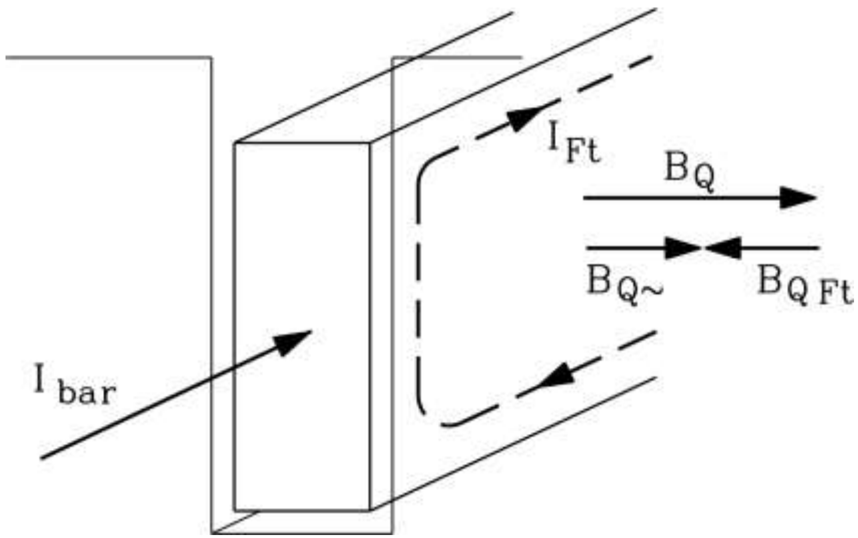
or

$$B_Q = \mu_0 \frac{I_{bar}}{b_r}, \quad x > h_{bar}$$

Eddy currents in slot conductor at AC current

- **Slot flux density** is pulsating with line frequency, penetrating the slot bar from the side. High slot bars form a "massive short circuit loop". *FARADAY´s law yields:* $\boldsymbol{B_Q}$ induces voltage $u_i = -d\Phi/dt$ in bar, which causes **eddy current flow $\boldsymbol{I_{Ft}}$.** Self field of that eddy current B_{QFt} is directed opposite to $\boldsymbol{B_Q}$ due to *LENZ´s rule*.

- Hence the **eddy current** I_{Ft} flows in upper bar region IN direction of bar current I_{bar} , and in lower bar region OPPOSITE to bar current.



- ***Facit 1:***

Due to I_{Ft} the resulting bar current density is HIGHER in upper bar region: **Current displacement towards upper bar region ("Skin effect").**

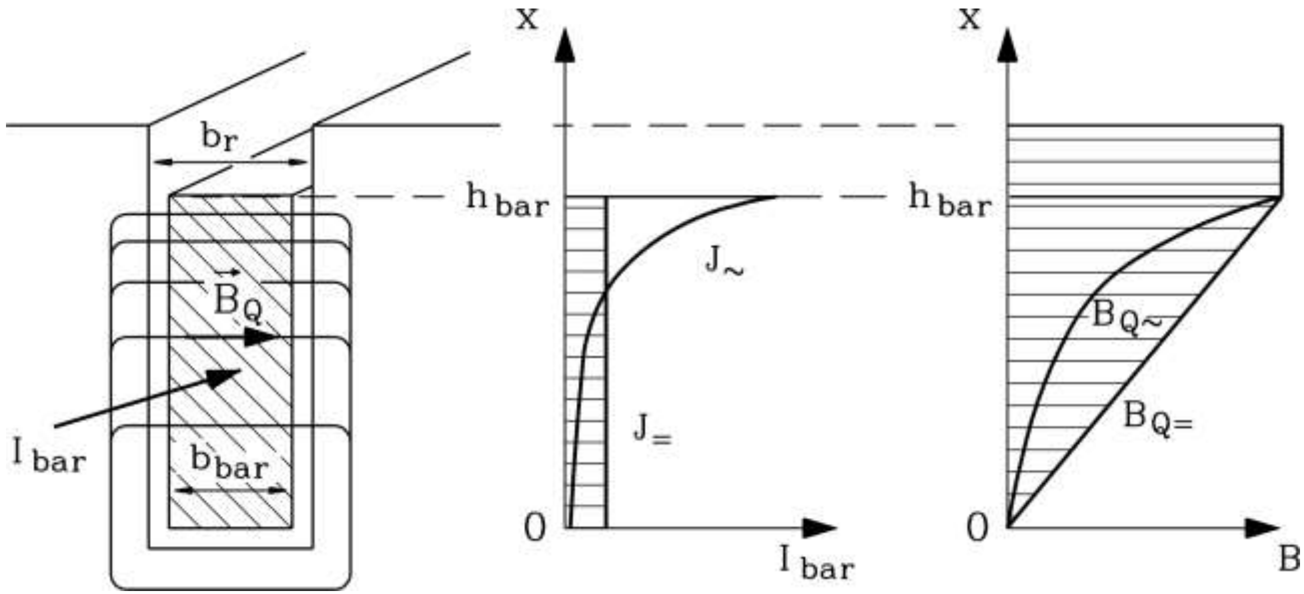
- ***Facit 2:***

The **resulting** slot stray flux density $B_{Q\sim}$ is due to B_{QFt} **reduced.**

- **Current displacement INCREASES** with increasing frequency f_r , with increasing electric bar-conductivity κ, with increasing bar height h_{bar} and with increasing permeability μ of conductor. (***Note:*** Copper and aluminium´s permeability is $\mu = \mu_0$!)

3. Eddy current losses in winding systems

Equivalent bar resistance and inductance at eddy currents

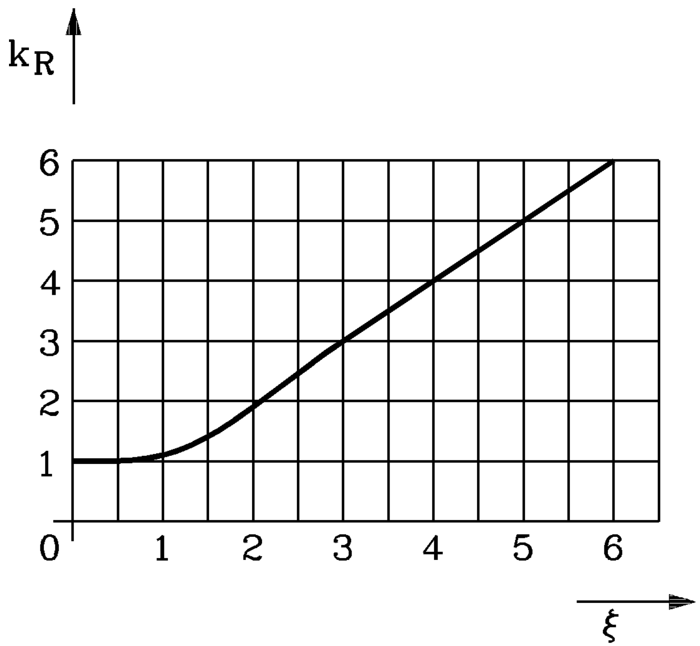


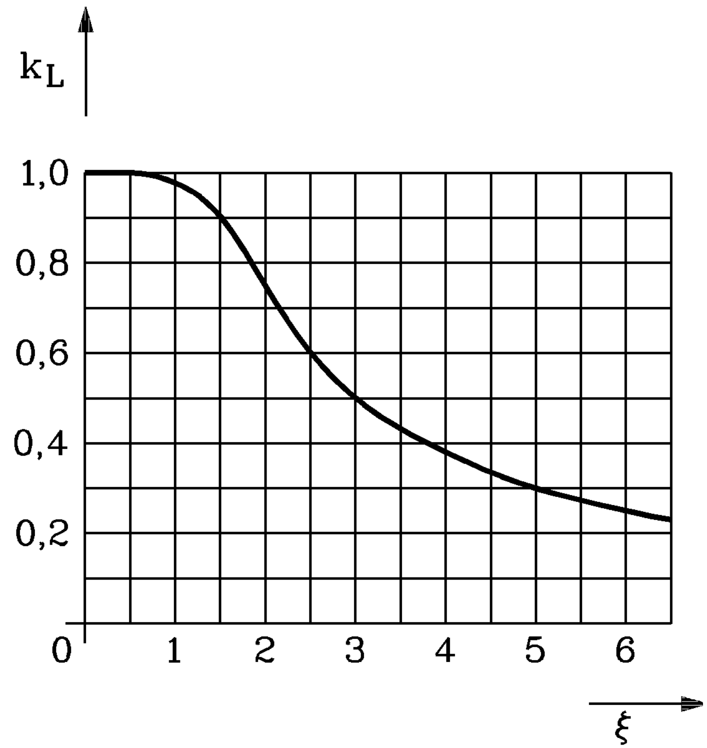
- Due to high stator frequency major part of bar current flows in upper bar region: so only reduced bar cross section is used for current flow. Thus "AC bar resistance" $R_{bar\sim}$ is higher than "DC bar resistance" $R_{bar=}$.

- Due to reduction of slot stray flux density the slot leakage flux is reduced. Hence the "AC bar inductance" $L_{bar\sim}$ is smaller than the "DC bar inductance" $L_{bar=}$.

$$\boxed{R_{bar\sim} = k_R R_{bar=} > R_{bar=}} \qquad \boxed{L_{\sigma,bar\sim} = k_L L_{\sigma,bar=} < L_{\sigma,bar=}}$$

Resistance increase k_R and inductance decrease k_L





"Reduced" conductor height ξ :
Per-unit value ξ, containing all relevant parameters:

$$\boxed{\xi = h_{bar}\sqrt{\pi f_s \mu \kappa \frac{b_{bar}}{b_s}}}$$

k_R, k_L for deep bar ("rectangular cross section") depend on ξ !

3. Eddy current losses in winding systems

• <u>Example:</u> **Current displacement in a slot copper bar:**

- At 75°C bar temperature copper conductivity is $\kappa_{Cu} = 50\cdot10^6$ S/m.
- Bar width = slot width: $b_{bar} = b_s$
- Permeability: $\mu_{Cu} = \mu_0 = 4\pi\cdot10^{-7}\,\mathrm{Vs/(Am)}$
- Stator frequency $f_s = 50$ Hz
- Bar height: $h_{bar} = 3$ cm

$$\xi = h_{bar}\sqrt{\pi f_s \mu\kappa\frac{b_{bar}}{b_s}} = 3\cdot10^{-2}\cdot\sqrt{\pi\cdot50\cdot4\pi\cdot10^{-7}\cdot50\cdot10^6\cdot1} = 2.98\approx3$$

From curve $k_R(\xi)$ we get: $k_R(3) = 3$ and from $k_L(\xi)$ follows: $k_L(3) = 0.5$.

• ***<u>Facit:</u>***

- Bar resistance increases up to 3-fold !

- Bar inductance decreases down to 50%.

• *Rule of thumb:*

At 50 Hz the increase of resistance of copper deep bar is $k_R = h_{bar}[cm]$.

Summary:

Basics on current displacement

- Slot conductor excites slot stray flux
- AC slot stray flux induces eddy currents in slot conductor
- Resulting conductor current density is displaced to the slot top
- Increase of equivalent conductor resistance due to eddy current losses
- Opposing self-flux of eddy currents reduces slot inductance

3. Eddy current losses in winding systems

3.1 Additional losses in electrical machines

3.2 Basics on current displacement

3.3 Current displacement in massive slot conductor

3.4 Critical conductor height

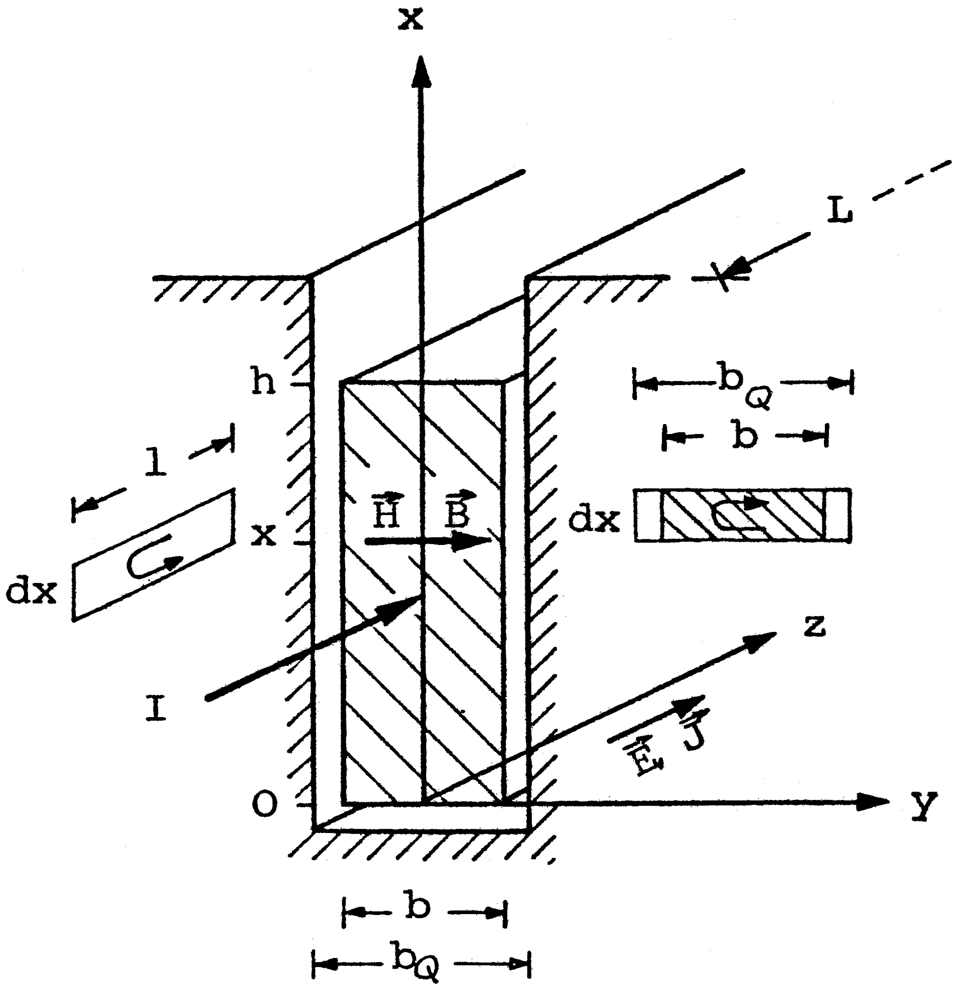
3.5 Use of current displacement in electrical machines

3.6 Methods to reduce current displacement effect

3.7 Air-gap winding for superconducting machines

3. Eddy current losses in winding systems

3.3 Current displacement in massive slot conductor



- ***Ampere´s law:***

$$\oint_C \vec{H} \bullet d\vec{s} = \Theta = \vec{J} \bullet \vec{A} = \kappa \vec{E} \bullet \vec{A}$$

$$-H_y(x) b_Q + H_y(x+dx) b_Q = \kappa E_z b dx$$

$$-H_y(x) b_Q + (H_y(x) + \frac{\partial H_y}{\partial x} dx) b_Q = \kappa E_z b dx$$

$$\boxed{\frac{\partial H_y}{\partial x} = \kappa \frac{b}{b_Q} E_z}$$

1. *Maxwell* equation

- ***Faraday´s law:*** $\oint_C \vec{E} \bullet d\vec{s} = u_i = -\frac{\partial \Phi}{\partial t}$

$$E_z(x) l - E_z(x+dx) l = -\mu l \cdot dx \cdot \frac{\partial H_y}{\partial t}$$

$$E_z(x) l - (E_z(x) + \frac{\partial E_z}{\partial x} dx) l = -\mu l \cdot dx \cdot \frac{\partial H_y}{\partial t}$$

$$\boxed{\frac{\partial E_z}{\partial x} = \mu \frac{\partial H_y}{\partial t}}$$

2. *Maxwell* equation

Calculation of eddy currents in slot conductor (1)

- Solution of linear partial differential equations for sinusoidal time functions: Use of complex phasors: yields conventional linear differential equation!

$$H(x,t) = \mathrm{Re}\left\{\underline{H}(x)\cdot\sqrt{2}\cdot e^{j\omega t}\right\},\ E(x,t) = \mathrm{Re}\left\{\underline{E}(x)\cdot\sqrt{2}\cdot e^{j\omega t}\right\},\ J(x,t) = \mathrm{Re}\left\{\underline{J}(x)\cdot\sqrt{2}\cdot e^{j\omega t}\right\}$$

$$H(x,t)\rightarrow\underline{H}(x),\ E(x,t)\rightarrow\underline{E}(x),\ J(x,t)\rightarrow\underline{J}(x)$$

$$\frac{\partial\underline{H}_y}{\partial x} = \kappa\frac{b}{b_Q}\underline{E}_z \qquad \frac{\partial\underline{E}_z}{\partial x} = j\omega\mu\underline{H}_y \quad \Rightarrow \quad \boxed{\frac{d^2\underline{E}_z(x)}{dx^2} - j\omega\mu\kappa\frac{b}{b_Q}\underline{E}_z(x) = 0}$$

- Solution of conventional linear differential equation: exponential functions !

$$\underline{E}_z(x) = \underline{C}e^{\underline{\lambda}x} \qquad \underline{\lambda}_{1,2} = \pm\sqrt{j\omega\mu\kappa\frac{b}{b_Q}} = \pm(1+j)\sqrt{\pi f\mu\kappa\frac{b}{b_Q}} = \pm(1+j)\beta$$

$$\boxed{\underline{E}_z(x) = \underline{C}_1 e^{-(1+j)\beta x} + \underline{C}_2 e^{(1+j)\beta x}} \qquad \beta = \sqrt{\pi f\mu\kappa\frac{b}{b_Q}}$$

Calculation of eddy currents in slot conductor (2)

$$\frac{\partial \underline{E}_z}{\partial x} = j\omega\mu \underline{H}_y \quad \Rightarrow \quad \underline{H}_y(x) = -\frac{1+j}{j}\cdot\frac{\beta}{\omega\mu}\left(\underline{C}_1 e^{-(1+j)\beta x} - \underline{C}_2 e^{(1+j)\beta x}\right)$$

Boundary conditions:

At lower bar edge (x = 0) magnetic field is zero: $\underline{H}_y(0) = 0$: $\underline{C}_1 = \underline{C}_2 = \underline{C}$.

$$\underline{H}_y(x) = \frac{1+j}{j}\cdot\frac{\beta}{\omega\mu}\cdot\underline{C}\left(-e^{-(1+j)\beta x} + e^{(1+j)\beta x}\right) = \frac{1+j}{j}\cdot\frac{\beta}{\omega\mu}\cdot\underline{C}\cdot 2\cdot sh[(1+j)\beta x]$$

At upper bar edge $x = h$ m.m.f. is equal to bar current $\underline{I}$; so magnetic field: $\underline{H}_y(x = h) = \underline{I}/b_Q$.

$$\underline{C} = \frac{j}{1+j}\cdot\frac{\omega\mu}{\beta b_Q}\cdot\frac{\underline{I}}{2\cdot sh[(1+j)\beta h]}$$

$$\boxed{\underline{H}_y(x) = \frac{\underline{I}}{b_Q}\cdot\frac{sh[(1+j)\beta x]}{sh[(1+j)\beta h]}}$$

$$\boxed{\underline{E}_z(x) = \frac{j}{1+j}\cdot\frac{\omega\mu}{\beta}\cdot\frac{\underline{I}}{b_Q}\cdot\frac{ch[(1+j)\beta x]}{sh[(1+j)\beta h]}}$$

$$\boxed{\underline{J}_z(x) = \kappa\underline{E}_z = \frac{j}{1+j}\cdot\frac{\omega\mu\kappa}{\beta}\cdot\frac{\underline{I}}{b_Q}\cdot\frac{ch[(1+j)\beta x]}{sh[(1+j)\beta h]}}$$

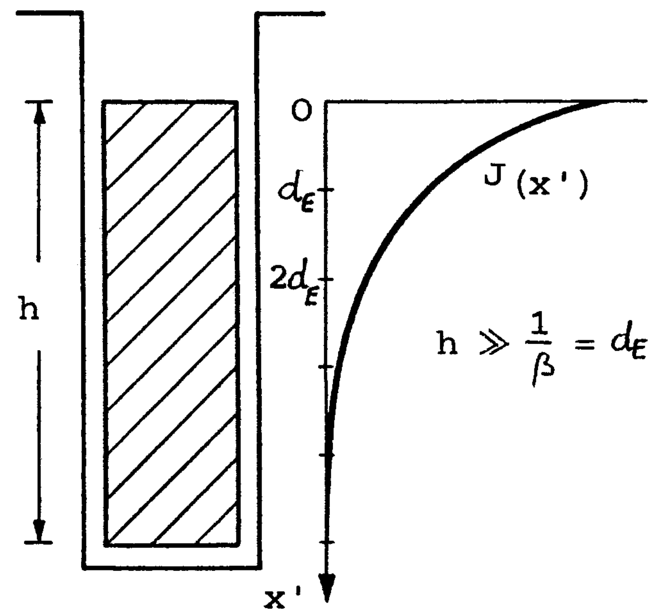
Current density distribution

- Absolute value of current density distribution J:

Use formulas: $\mathrm{sh}\,(x + jy) = \mathrm{sh}\,x \cos y + j\,\mathrm{ch}\,x \sin y$

$\mathrm{ch}\,(x + jy) = \mathrm{ch}\,x \cos y + j\,\mathrm{sh}\,x \sin y$

$$J_z(x) = \frac{1}{\sqrt{2}} \cdot \frac{\omega\mu\kappa}{\beta} \cdot \frac{I}{b_Q} \cdot \sqrt{\frac{ch2\beta x + \cos 2\beta x}{ch2\beta h - \cos 2\beta h}}$$



- Simplified expression for big β: $h >> 1/\beta$:

$\cos(2\beta h) << \mathrm{ch}(2\beta h)$, $x' = h - x$,

$$ch(2\beta \cdot x) = (e^{2\beta \cdot x} + e^{-2\beta \cdot x})/2 \approx e^{2\beta \cdot x}/2$$

$$\sqrt{ch(2\beta \cdot x)/ch(2\beta \cdot h)} \approx \sqrt{e^{2\beta \cdot x}/e^{2\beta \cdot h}} = e^{\beta(x-h)} = e^{-\beta \cdot x'}$$

$$J_z(x') = \frac{1}{\sqrt{2}} \cdot \frac{\omega\mu\kappa}{\beta} \cdot \frac{I}{b_Q} \cdot e^{-\beta \cdot x'}$$

Penetration depth d_E

$$d_E = \frac{1}{\beta} = \sqrt{\frac{b_Q}{b} \cdot \frac{1}{\pi f \mu\kappa}}$$

3. Eddy current losses in winding systems

Increased losses due to eddy currents

- Total losses in conductor with length *L*: $P_1 = \frac{b \cdot L}{\kappa} \cdot \int_0^h J_z^2 dx = I^2 R_\sim = k_R \cdot I^2 R_0$

- DC resistance of conductor: $R_0 = \frac{L}{bh\kappa}$

$$P_1 = \frac{b \cdot L}{\kappa} \cdot \int_0^h \frac{1}{2} \left(\frac{\omega\mu\kappa}{\beta} \right)^2 \cdot \left(\frac{I}{b_Q} \right)^2 \cdot \frac{\cosh(2\beta x) + \cos(2\beta x)}{\cosh(2\beta h) - \cos(2\beta h)} dx = I^2 \cdot R_0 \cdot \xi \cdot \frac{\sinh 2\xi + \sin 2\xi}{\cosh 2\xi - \cos 2\xi}$$

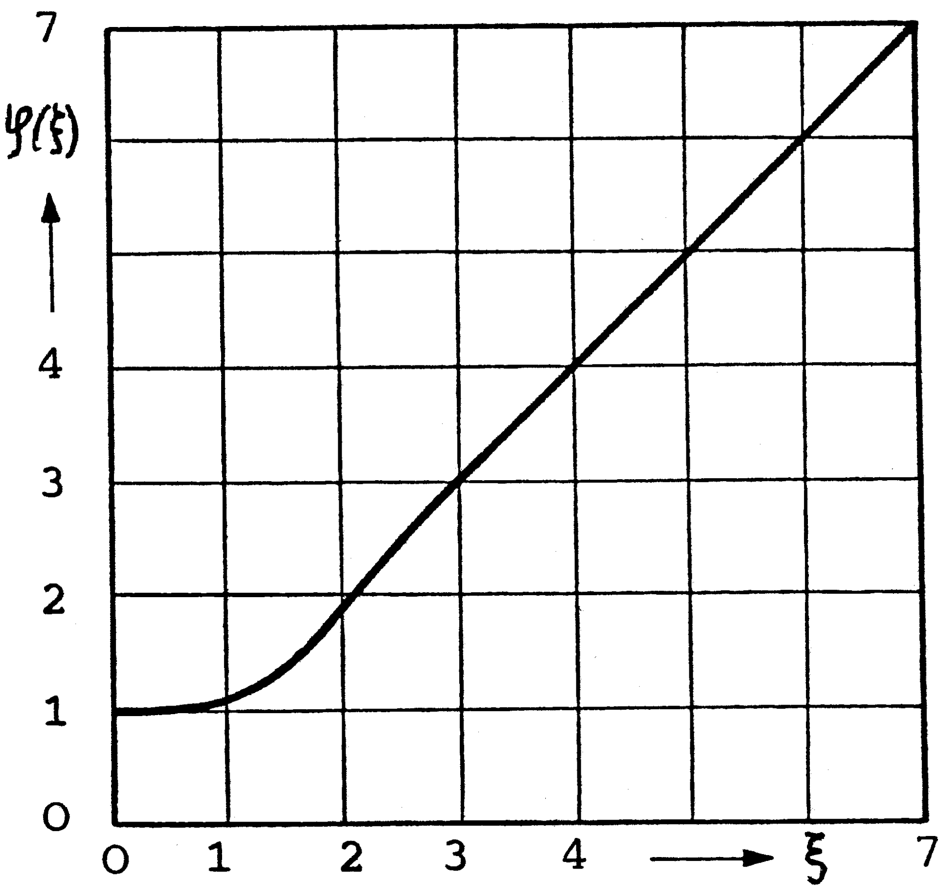
- Increased losses by coefficient: $\boxed{k_R = \frac{R_\sim}{R_0} = \varphi(\xi) = \xi \cdot \frac{\sinh 2\xi + \sin 2\xi}{\cosh 2\xi - \cos 2\xi}}$

Abbreviation: "Reduced" conductor height: $\xi = \beta \cdot h = \frac{h}{d_E} = h \cdot \sqrt{\pi f \mu \kappa \frac{b}{b_Q}}$

- Above $h > 0.5\, d_E$ current displacement is significant, rising above $\xi = 3$ with nearly linear increase $k_R \cong \xi$.

3. Eddy current losses in winding systems

Increased losses in massive slot conductor



$$k_R = \frac{R_\sim}{R_0} = \varphi(\xi) = \xi \cdot \frac{\sinh 2\xi + \sin 2\xi}{\cosh 2\xi - \cos 2\xi}$$

$\xi > 3$:

$$R_\sim = k_R R_0 \approx \xi R_0 = \frac{h}{d_E} \cdot \frac{L}{bh\kappa} = \frac{L}{bd_E\kappa}$$

3. Eddy current losses in winding systems

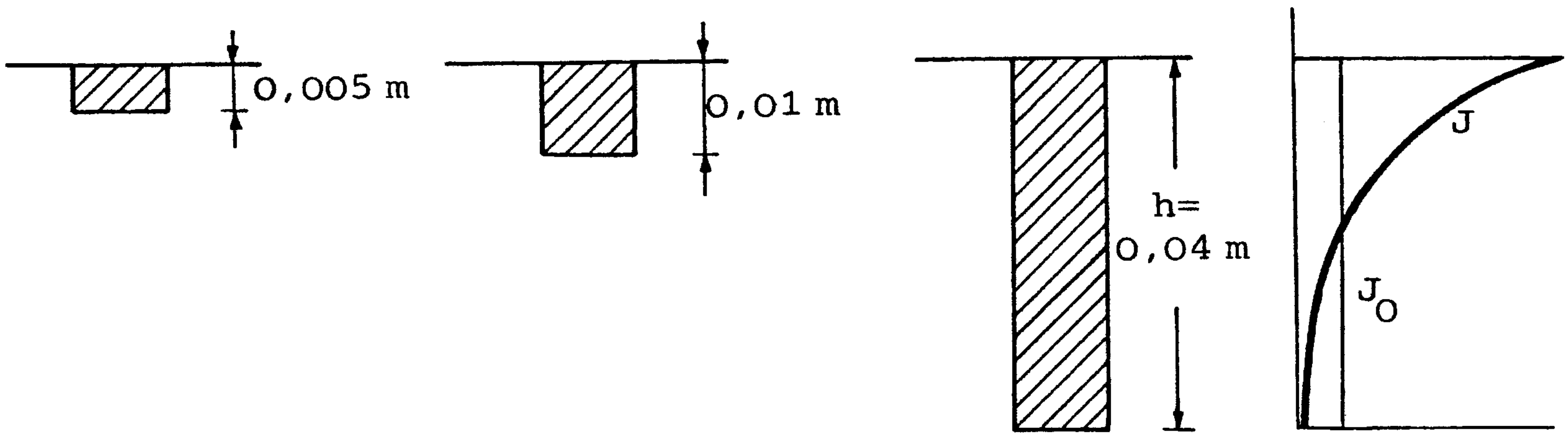
Effect of increased losses for copper bar

Example:

Cu-bar with different height h at f = 50 Hz:

h: a) 5 mm, b) 10 mm, c) 40 mm

$\kappa = 50\cdot 10^6$ 1/m, $\mu = \mu_0 = 4\cdot\pi\cdot 10^{-7}$ Vs/(Am), $b/b_Q = 1$, $d_E = 0.01$ m = 10 mm



$\xi = \dfrac{0,005}{0,01} = 0,5$ $\qquad$ $\dfrac{0,01}{0,01} = 1,0$ $\qquad$ $\dfrac{0,04}{0,01} = 4$

$\boxed{k \approx 1,0}$ $\qquad$ $\boxed{k = 1,09}$ $\qquad$ $\boxed{k = 4,0}$ $\qquad$ **Increase of losses**

3. Eddy current losses in winding systems

Instantaneous current density distribution (1)

At different instants *t* : Current changes sinusoidal: $i(t) = \sqrt{2} \cdot I \cdot \cos \omega t$ **:**

$$\underline{J}_z(x) = \kappa E_z = \frac{j}{1+j} \cdot \frac{\omega\mu\kappa}{\beta} \cdot \frac{I}{b_Q} \cdot \frac{ch[(1+j)\beta x]}{sh[(1+j)\beta h]} = J_{re}(x) + jJ_{im}(x)$$

$$J_z(x,t) = \mathrm{Re}\left\{\underline{J}_z(x) \cdot \sqrt{2} \cdot e^{j\omega t}\right\} = \sqrt{2} \cdot (J_{re}(x) \cdot \cos\omega t - J_{im}(x) \cdot \sin\omega t)$$

Example:

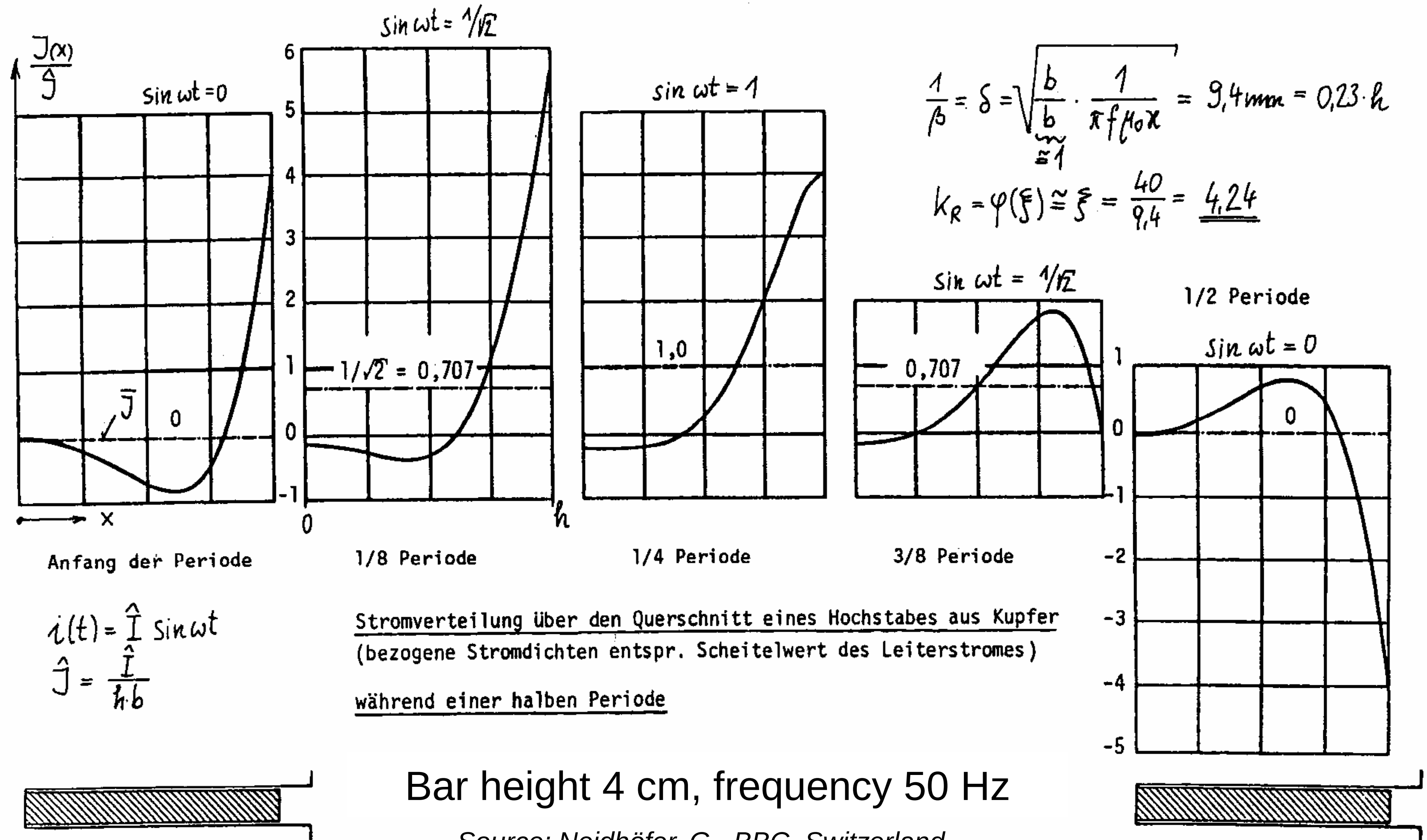
Copper bar, *h* = 4 cm, *f* = 50 Hz, b/b_Q = 1, $\kappa = 50 \cdot 10^6$ **S/m,** $d_E = 1/\beta = 10$ **mm,** $\xi = 4.0$ **.**

Current density $J_z(x,t)$ for $0 \le x \le h$: per unit of DC current density $J = I/(bh)$ **:**

Begin of period	***i* = 0**	$\omega t = -\pi/2$
1/8 period	$i = \hat{I}/\sqrt{2}$	$\omega t = -\pi/4$
1/4 period	$i = \hat{I}$	$\omega t = 0$
3/8 period	$i = \hat{I}/\sqrt{2}$	$\omega t = \pi/4$
Half period	***i* = 0**	$\omega t = \pi/2$

3. Eddy current losses in winding systems

Instantaneous current density distribution (2)

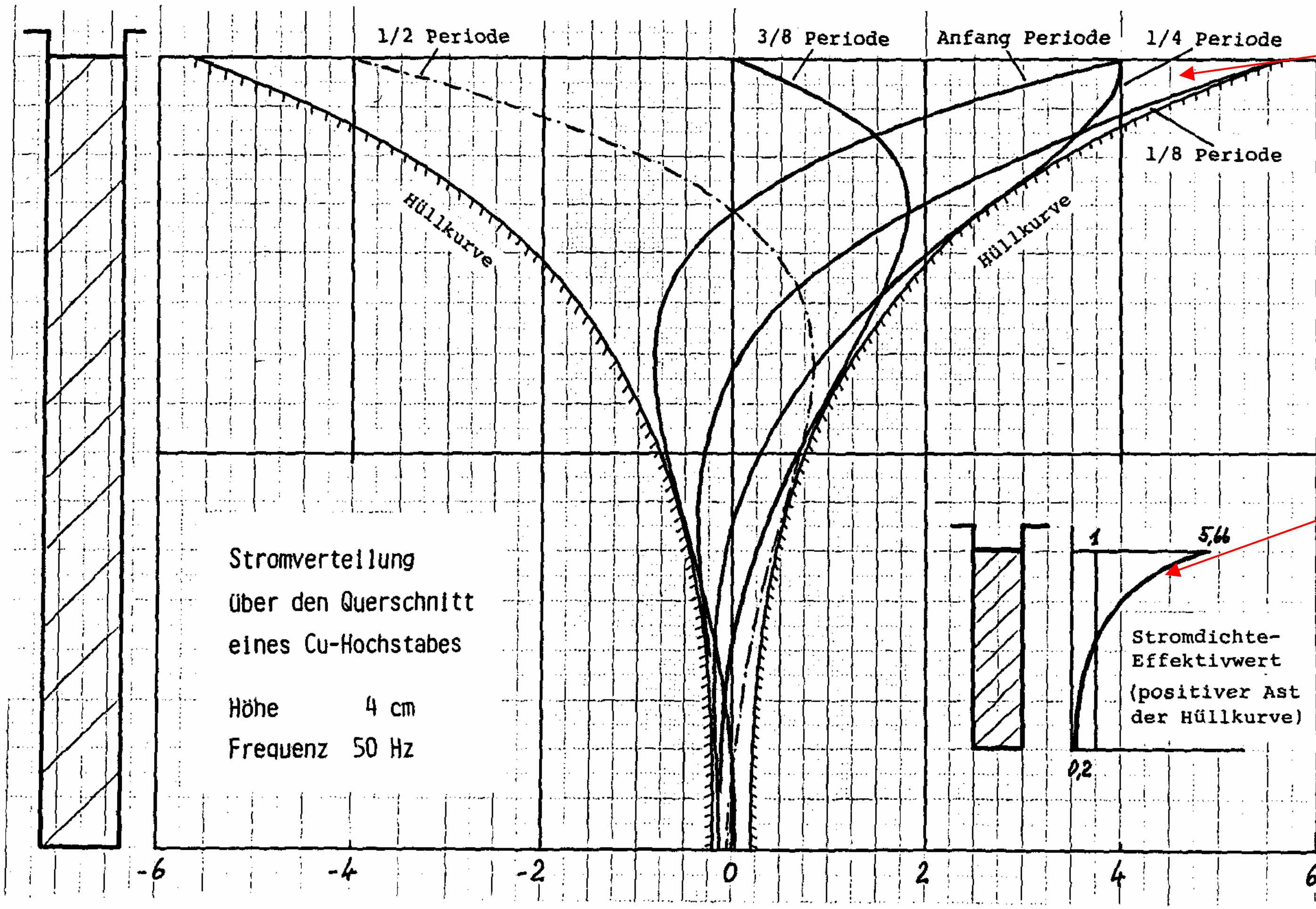


Bar height 4 cm, frequency 50 Hz

Source: Neidhöfer, G., BBC, Switzerland

3. Eddy current losses in winding systems

Instantaneous current density distribution (3)



- Current density distribution along deep bar for 0, 1/8, ¼, 3/8, ½ period

- Copper bar

- bar height 4 cm, frequency 50 Hz,

- The envelope of all instantaneous current density distribution is the resulting absolute value of current density distribution

Source: Neidhöfer, G., BBC, Switzerland

3. Eddy current losses in winding systems

Losses in massive conductive parts (1)

- If tangential AC field strength H_t at surface of body is given, with big body thickness $h >> \beta$ (e.g. thick plate), we get from previous solution:

$$J_z = \frac{1}{\sqrt{2}} \cdot \frac{\omega\mu\kappa}{\beta} \cdot \frac{I}{b_Q} \cdot e^{-\beta \cdot x'} = \frac{H_t}{d_E} \cdot e^{-x'/d_E}$$

- Losses : (e.g. in thick plate): $P_1 = A \cdot \int_0^\infty \frac{J_z^2}{\kappa} \cdot dx' = A \cdot \frac{H_t^2}{2} \cdot \sqrt{\frac{\pi f \mu}{\kappa}}$

Losses per surface e.g. of plate: $\boxed{\frac{P_1}{A} = \frac{H_t^2}{2\kappa} \cdot \frac{1}{d_E}}$

- Losses are small: a) if penetration depth is big,

b) if conductivity is big.

3. Eddy current losses in winding systems

Losses in massive conductive parts (2)

Material	κ / S/m	d_E / mm	P_1/A (per unit losses)
Copper	$50 \cdot 10^6$	10	1.0
Aluminium	$29 \cdot 10^6$	13	1.32
Iron, steel (μ_r = 100)	$4 \cdot 10^6$	3.5	35.7
Iron, steel (μ_r = 1000)	$4 \cdot 10^6$	1.1	113.6
Non-magnetic steel (μ_r = 1)	$1.5 \cdot 10^6$	57.5	5.8

Penetration depth and eddy current losses at *f* = 50 Hz, 55°C !

Application:

- Copper plate for electro-dynamic press plate shielding.

- Aluminium or non-magnetic steel press plates instead of magnetic iron press plates

3. Eddy current losses in winding systems

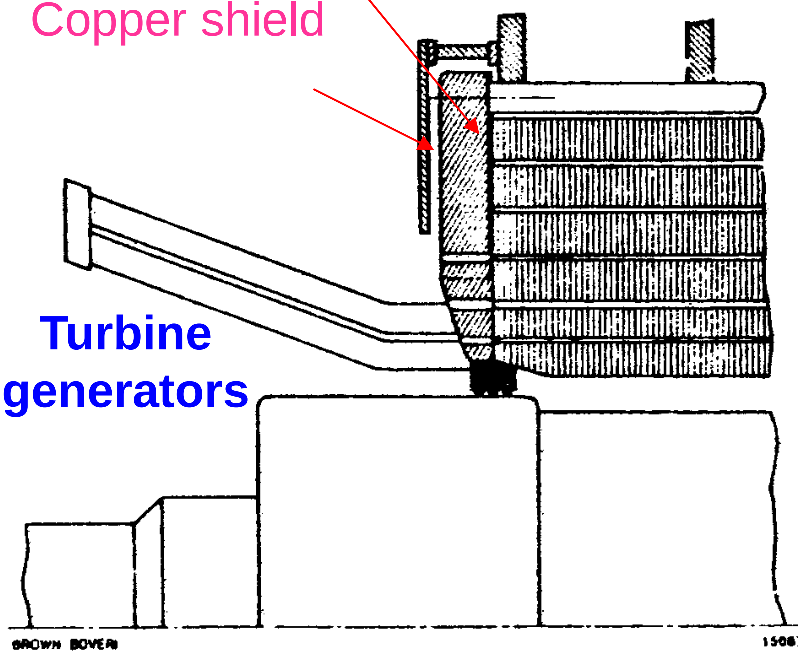
Press plate losses

Axial end field component induces with stator frequency eddy currents in press plates

Press plate

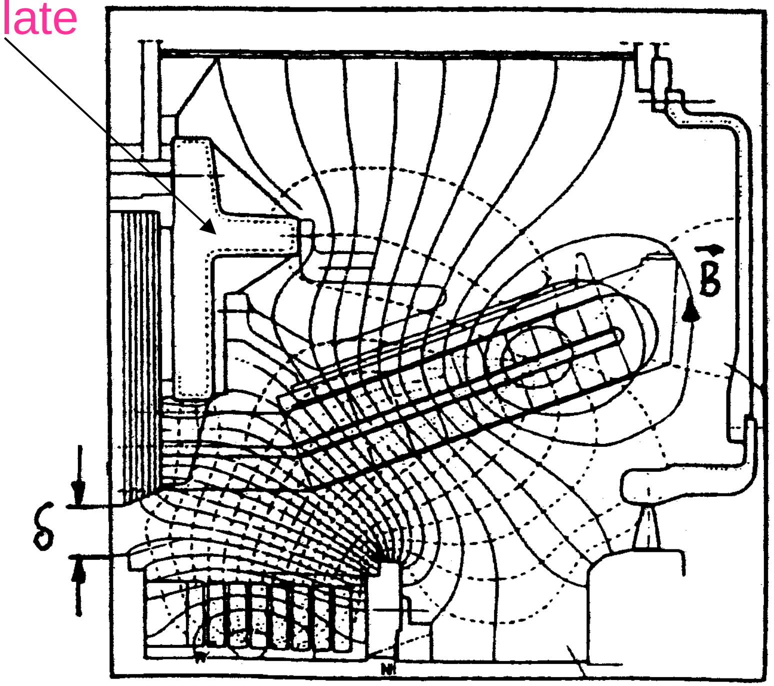
Copper shield

Turbine generators



No-load

Press plate



Load

Source:
Neidhöfer, G. & Darrieux, G., BBC, Switzerland

Summary:

Current displacement in massive slot conductor

- Slot flux calculation due to slot conductor via MAXWELL´s equations
- Derivation of reduced conductor height, equivalent resistance and resulting slot inductance
- Loss formula may be used as a rough estimate also for press plates, but only due to tangential flux density

3. Eddy current losses in winding systems

3. Eddy current losses in winding systems

3.4 Critical conductor height

a) Ohmic losses:

$$P_0 = I^2 R_0 = \frac{I^2 L}{b\kappa h} = \frac{I^2 L}{b d_E \kappa} \cdot \frac{d_E}{h} = \frac{P_{0d_E}}{\xi}$$

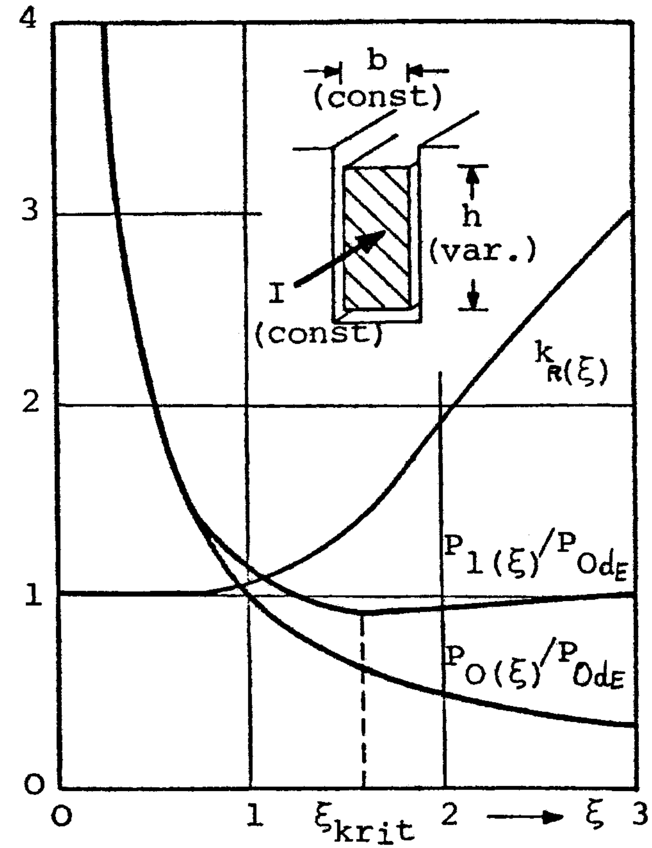
b) AC losses:

$$P_1 = I^2 R_\sim = I^2 R_0 \frac{R_\sim}{R_0} = P_0 k_R = P_{0d_E} \cdot \frac{sh(2\xi) + \sin(2\xi)}{ch(2\xi) - \cos(2\xi)}$$

- With increasing conductor height at given current a) decreases, but b) increases. Where is optimum ? Differentiation:

$dP_1/d\,\xi = 0$ yields $sh(2\xi) \cdot \sin(2\xi) = 0$ at

$$\xi_{crit} = \frac{\pi}{2} = 1.57$$



Source: Neidhöfer, G., BBC, Switzerland

3. Eddy current losses in winding systems

Minimum "massive" bar conductor losses

- Minimum total losses at critical conductor height: optimum coefficient:

$$k_{R,opt} = \varphi(\xi_{crit}) = \varphi(\pi/2) = 1.44$$

Example:

Cu-conductor, f = 50 Hz: $\Rightarrow d_E = 0.01$ m: $h_{krit} = 0.0157$ m.

- How big are total losses for infinite conductor height ? FINITE !

$$P_1(\xi \to \infty) \approx P_{0d_E} \cdot th(2\xi) = P_{0d_E}$$

$$\boxed{P_{0d_E} = \frac{I^2 L}{b d_E \kappa}}$$

Facit:

For big machines (big current = big conductor cross section) it is necessary to split conductor into smaller strands to avoid excessive AC losses !

Summary:

Critical conductor height

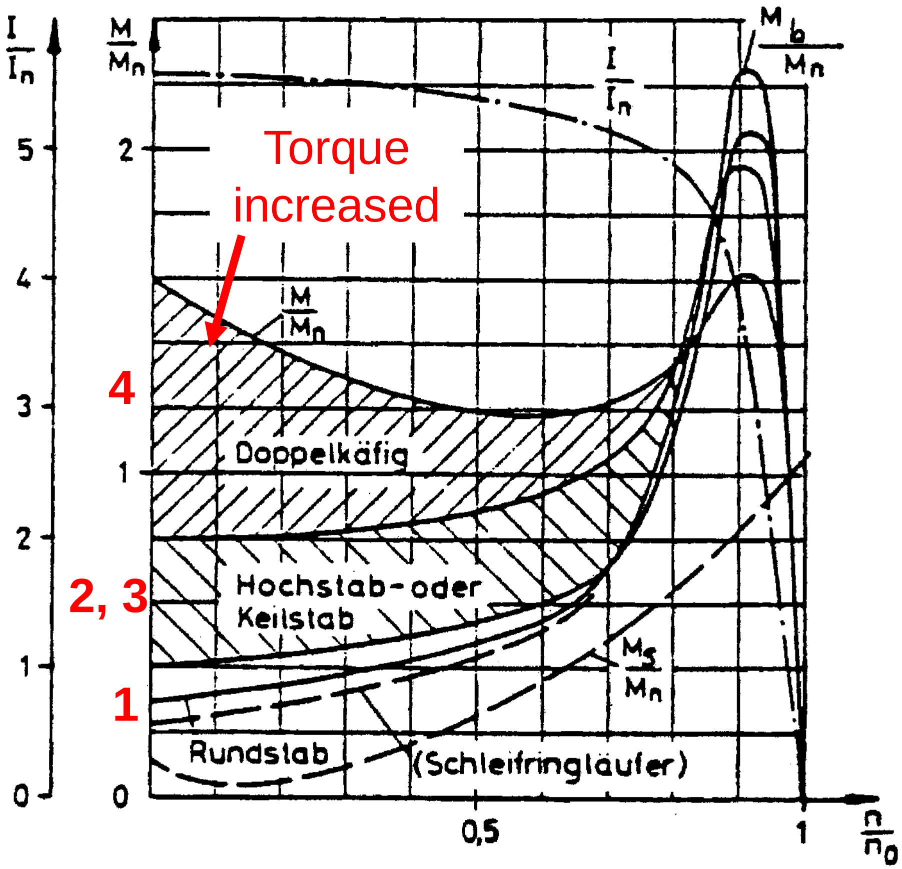
- Eddy currents in a massive slot conductor limit the useful conductor height
- At 50 Hz: Copper bar height bigger than 15 mm yields increased losses, although the cross section increases
- Necessity for other solutions to increase the slot conductor current

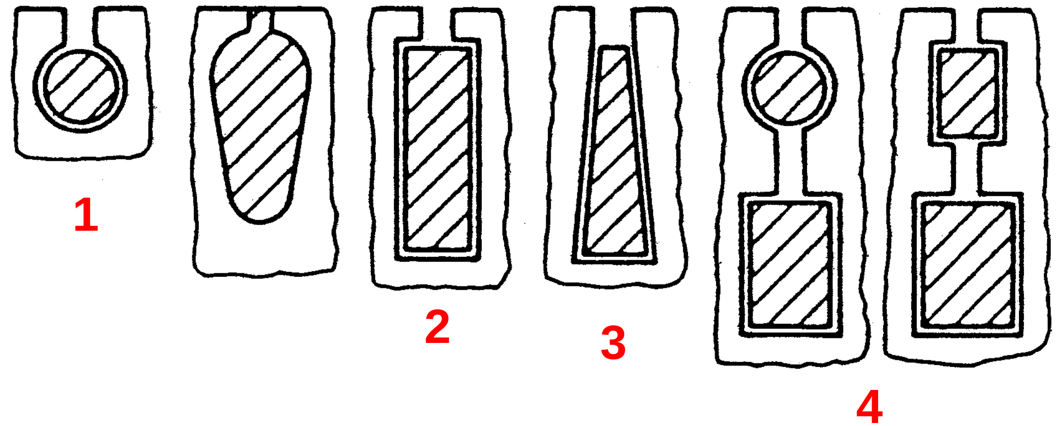
3. Eddy current losses in winding systems

3. Eddy current losses in winding systems

3.5 Use of current displacement in electrical machines

Increase of asynchronous starting torque in induction machines





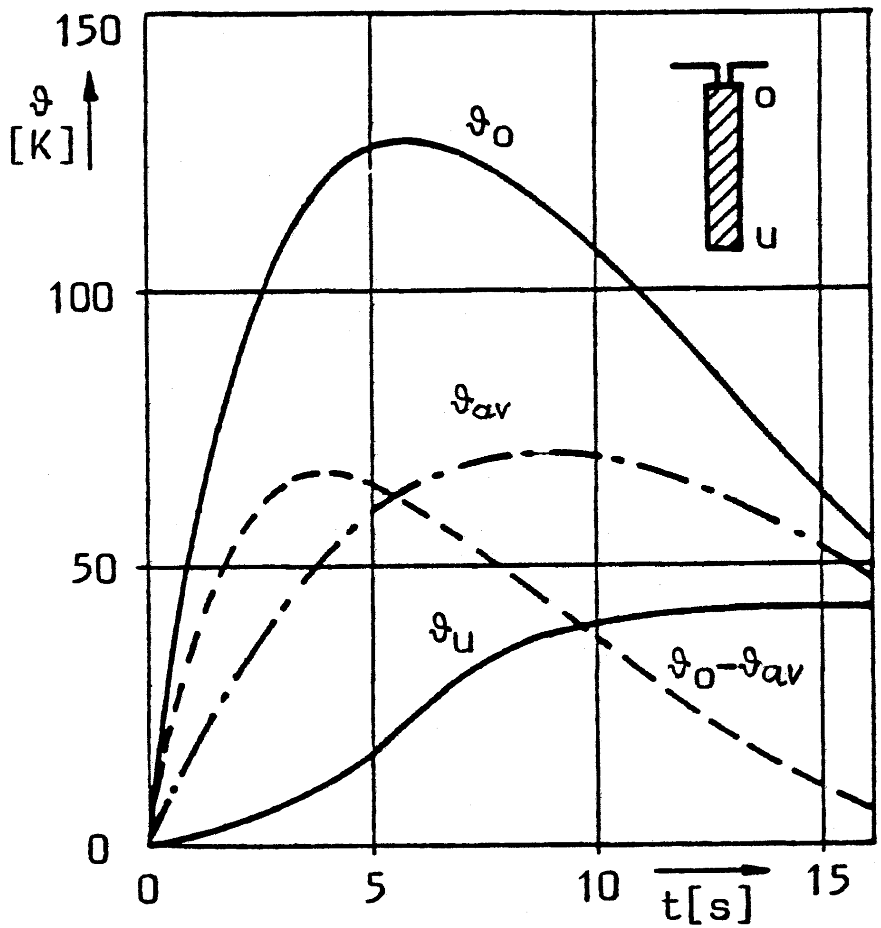
- Asynchronous starting torque due to rotor cage is directly proportional to rotor losses.

- So at stand still = big rotor frequency - big AC losses (with bar shapes 2, 3, 4) yield big torque increase !

Source: Bohn, T. (Ed.), TÜV-Rheinland

3. Eddy current losses in winding systems

Heating of rotor bar during asynchronous start-up



Source: Neidhöfer, G., BBC, Switzerland

Calculated temperature distribution in deep bar

- At upper bar edge much bigger heating due to current displacement

- Big machines need long time to run up (5 ... 20 s), so equalizing of temperature distribution due to heat conduction in bar

- Big bar temperature causes thermal expansion of hot copper:

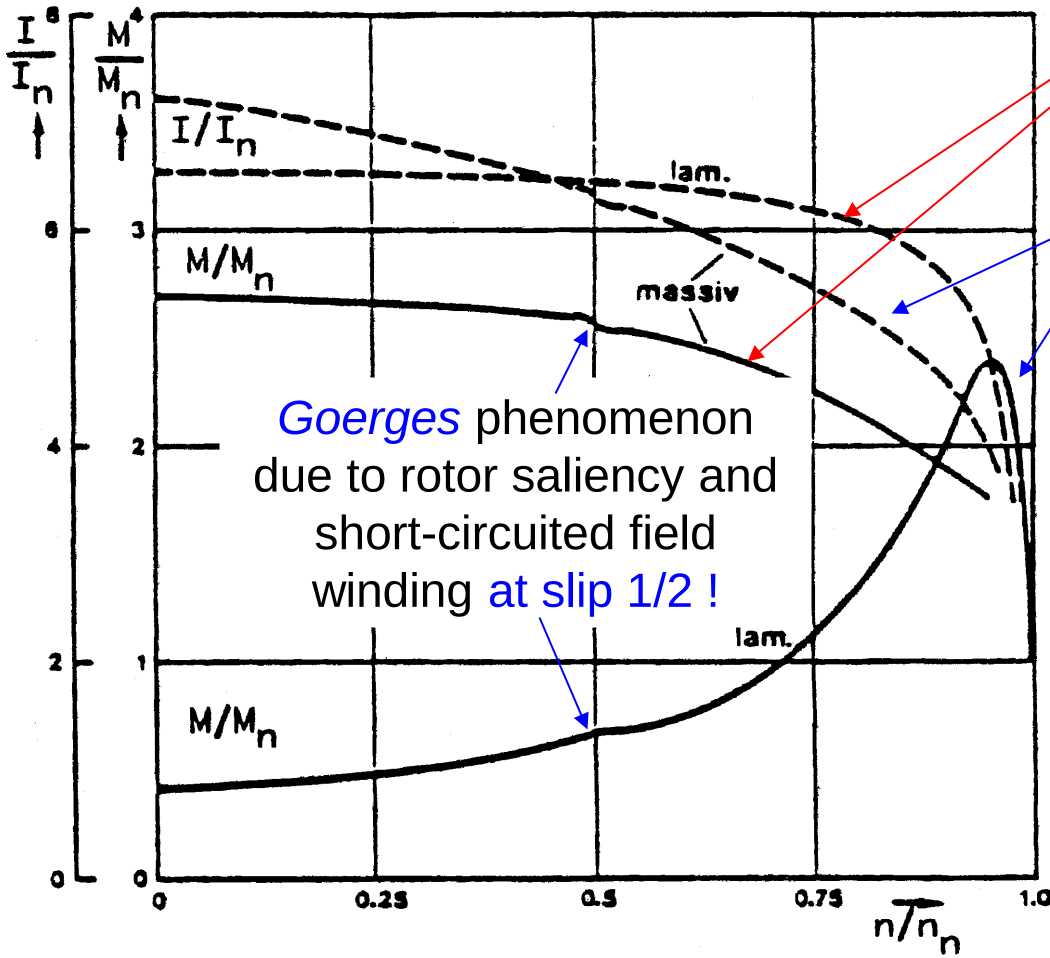
a) bar may be quenched out of slot

b) bar-ring welding may tear off !

- Cages are heat sensitive !

3. Eddy current losses in winding systems

Asynchronous start-up of synchronous motors



- Laminated rotor poles need starting copper cage (= heat sensitive)

- Massive rotor poles doe not need rotor cage: massive pole surface (conductive iron) is carrying eddy currents

Advantages:

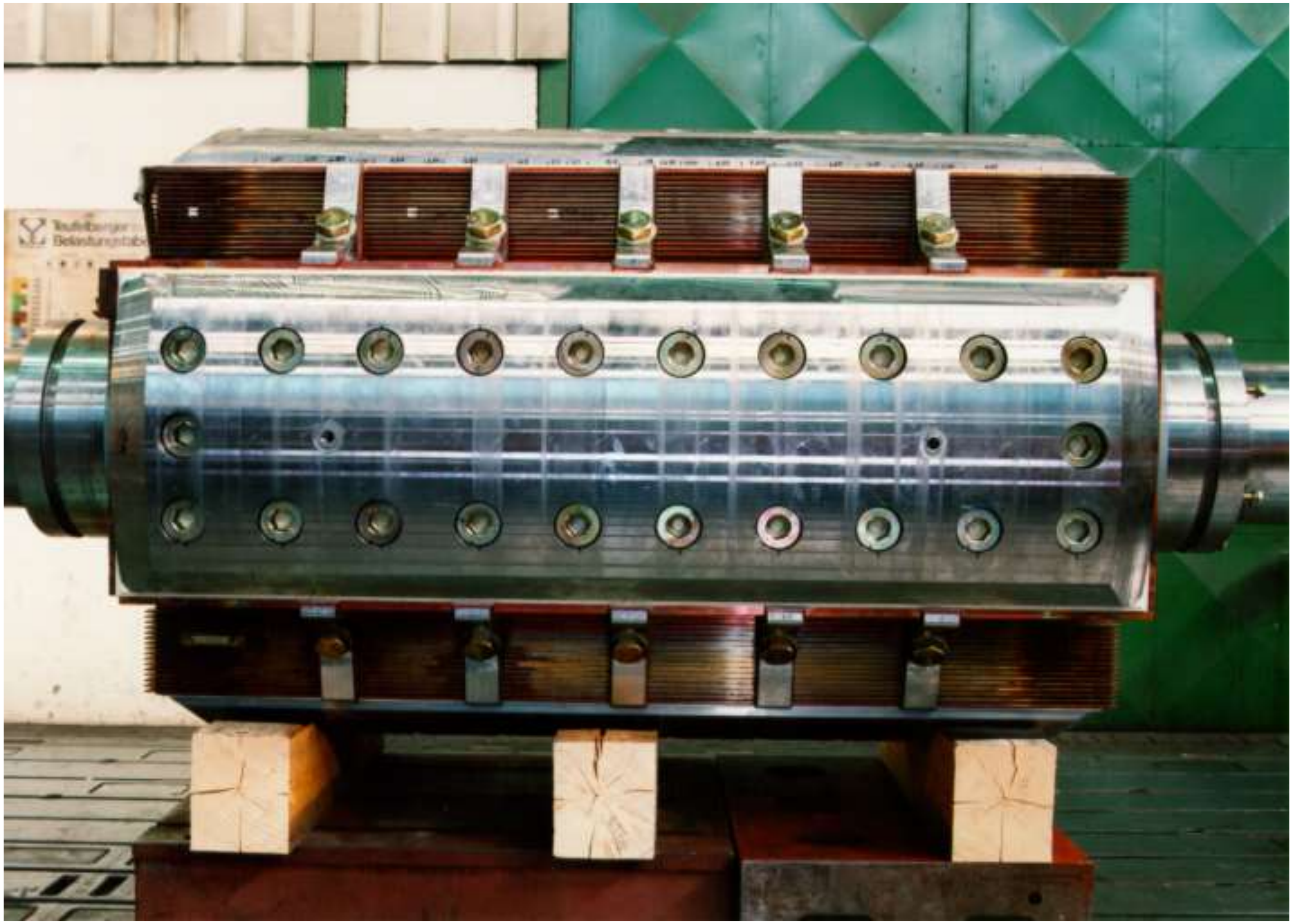
a) no heat expansion problem of cage !

b) 10 ... 20 times bigger iron rotor resistance shifts break down slip to nearly unity = much bigger starting torque.

Source: Bohn, T. (Ed.), TÜV Rheinland

3. Eddy current losses in winding systems

Massive pole synchronous motors



4 pole motor

Screwed poles

Source: Andritz Hydro, Austria

Summary:

Use of current displacement in electrical machines

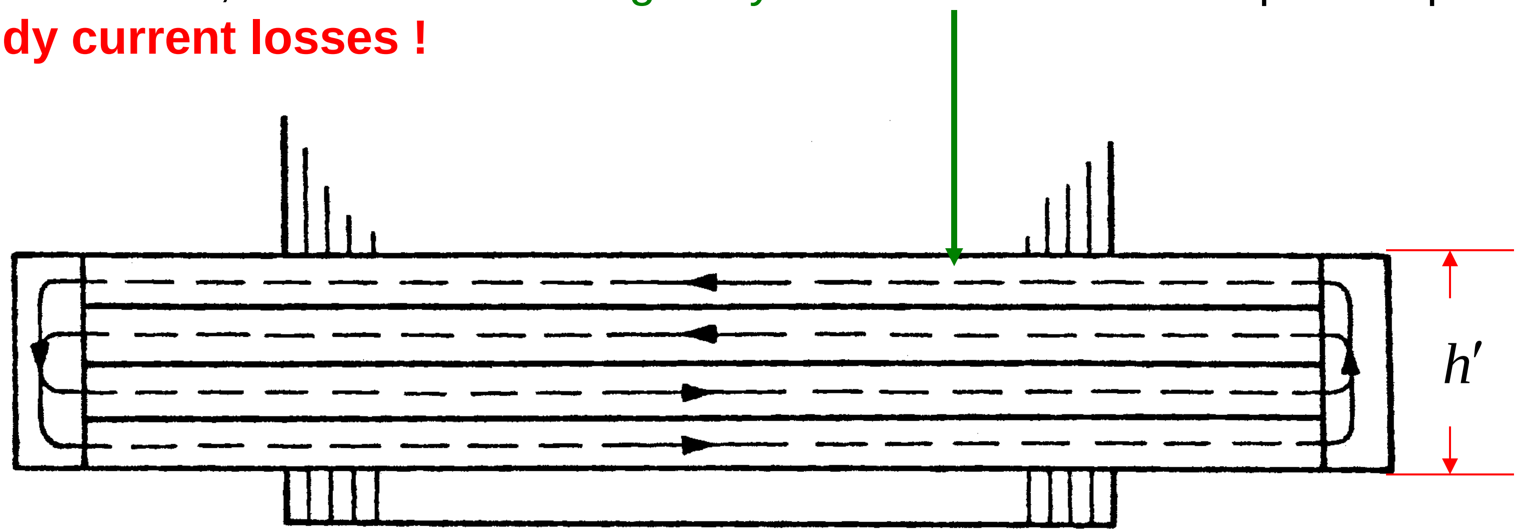
- Eddy currents in rotor bar yield increased asynchronous starting torque
- „Starting“ cage for synchronous machines
- Massive steel pole shoes also may be used as „starting“ and „damper“ cage

3. Eddy current losses in winding systems

3. Eddy current losses in winding systems

3.6 Methods to reduce current displacement effect

- Separating massive conductor into several parallel strands DOES NOT LEAD to reduction of AC losses, because circulating eddy currents will occur via parallel paths = **1st order eddy current losses !**



- Eddy currents have to flow also via overhang length, so effective conductivity is decreased by $l_{Fe}/(l_{Fe} + l_b)$, but total conductor height h' is active !

$$\xi = h' \cdot \sqrt{\pi f \mu \kappa \cdot \frac{l_{Fe}}{l_{Fe} + l_b} \cdot \frac{b}{b_Q}}$$

- *Facit:* Twisting is also needed !

Source: Neidhöfer, G., BBC, Switzerland

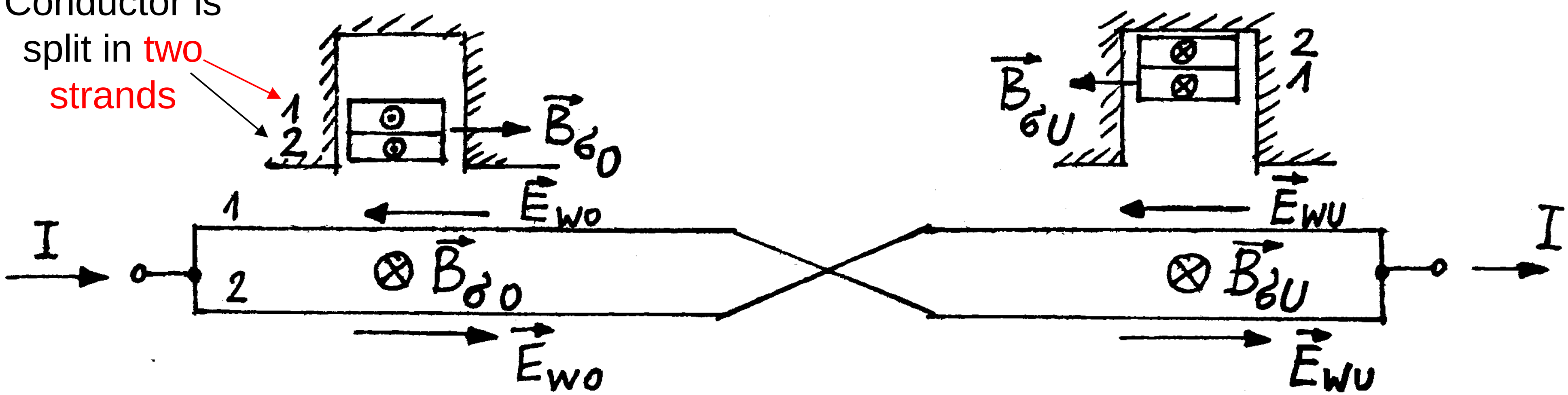
Transposition of strands in two slots

- Slot stray flux linkage in both coils opposite, so

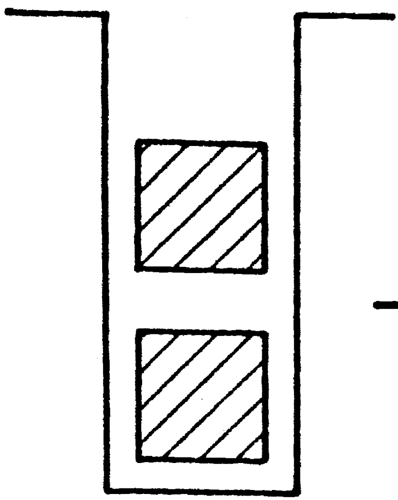
a) in single layer winding cancelling of stray flux = NO 1st order eddy current losses !
$B_{\sigma o} = B_{\sigma u}$: induced electric field E_{wo} = - E_{wu} : total $E_w = E_{wo} + E_{wu} = 0$!

b) in two layer winding stray flux in upper and lower layer different, so only reduction of total stray flux linkage ($B_{\sigma o} > B_{\sigma U}$) = reduction, but not full elimination of 1st order eddy current losses !

Conductor is split in two strands

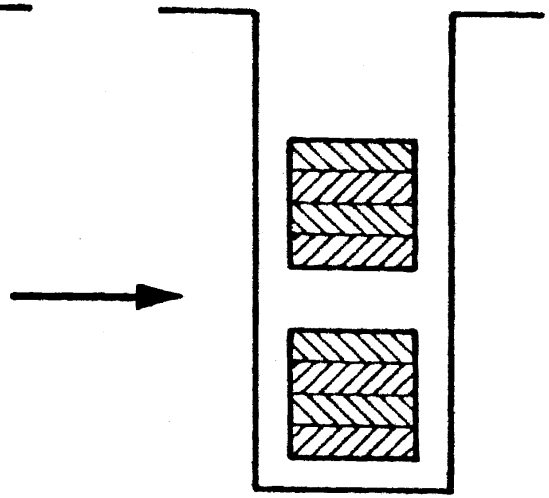


Transposition of strands in form wound coils



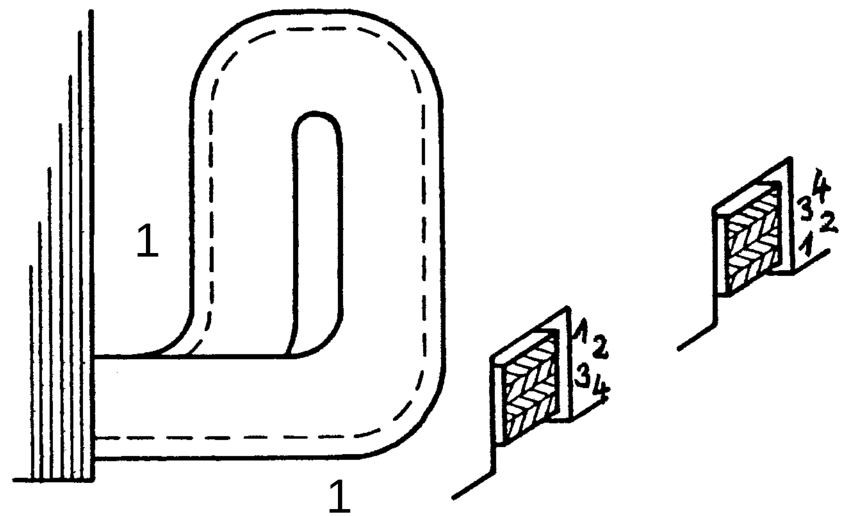
Two-layer

massive bars



Two-layer

4 strands per bar

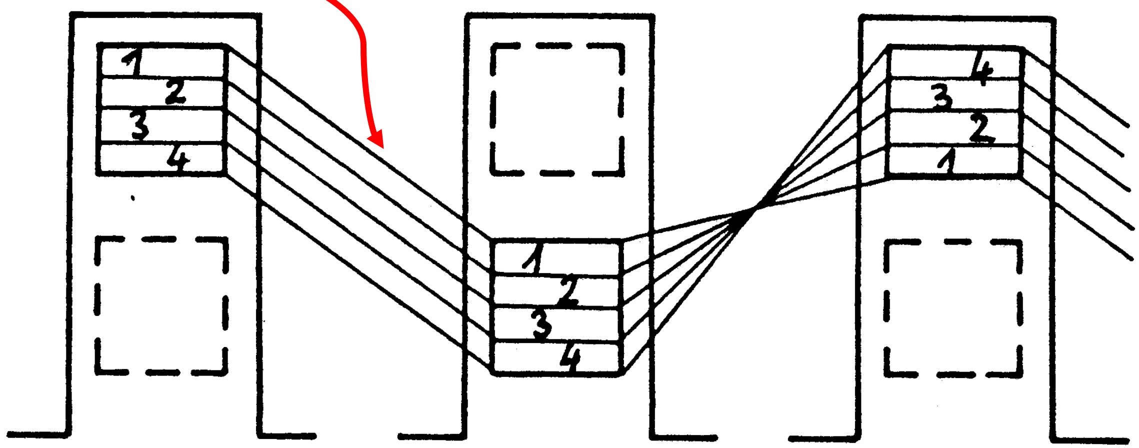


Two-layer form wound coil automatically changes position of strands in slots, so that reduction of stray flux is achieved !

Source: Neidhöfer, G., BBC, Switzerland

Transposition of strands in series-connected form wound coils

Series connection of the strands of two coils !



2nd coil lower layer

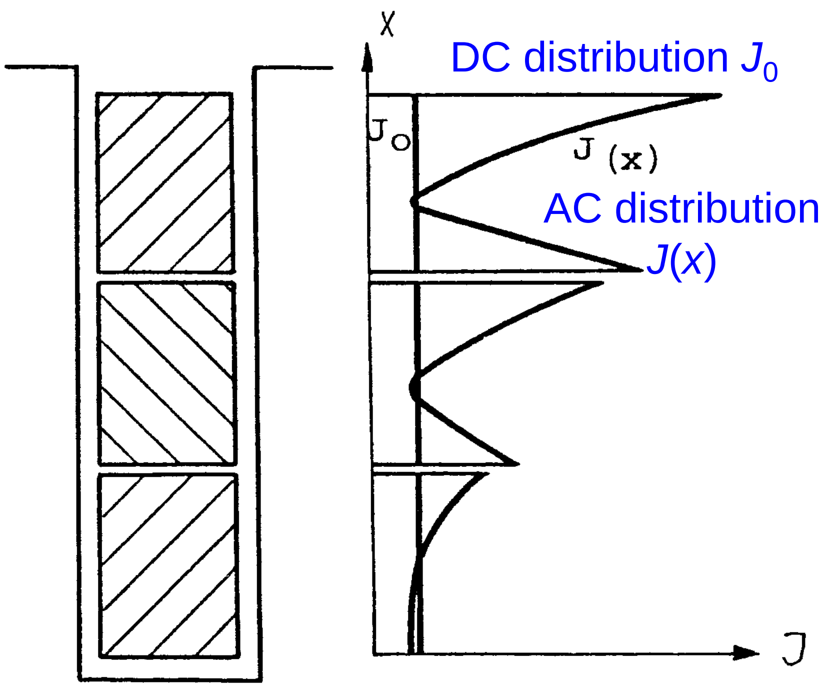
1st coil lower and upper layer

Source: Neidhöfer, G., BBC, Switzerland

- By connecting only the strands of series-connected two coils without paralleling the strands a complete elimination of slot stray flux is possible also for two-layer winding.

- But this is time-consuming, expensive manufacturing !

2^{nd} order eddy current losses



Coils with $N_c > 1$ number of turns:

- Each turn is a massive conductor

- The lowest conductor experiences only its own slot stray flux: $k_{R,1} = \varphi(\xi)$

- The next conductor experiences its own stray flux and the stray flux, excited by the turn below !

$$k_{R,2} = \varphi(\xi) + 2\psi(\xi)$$

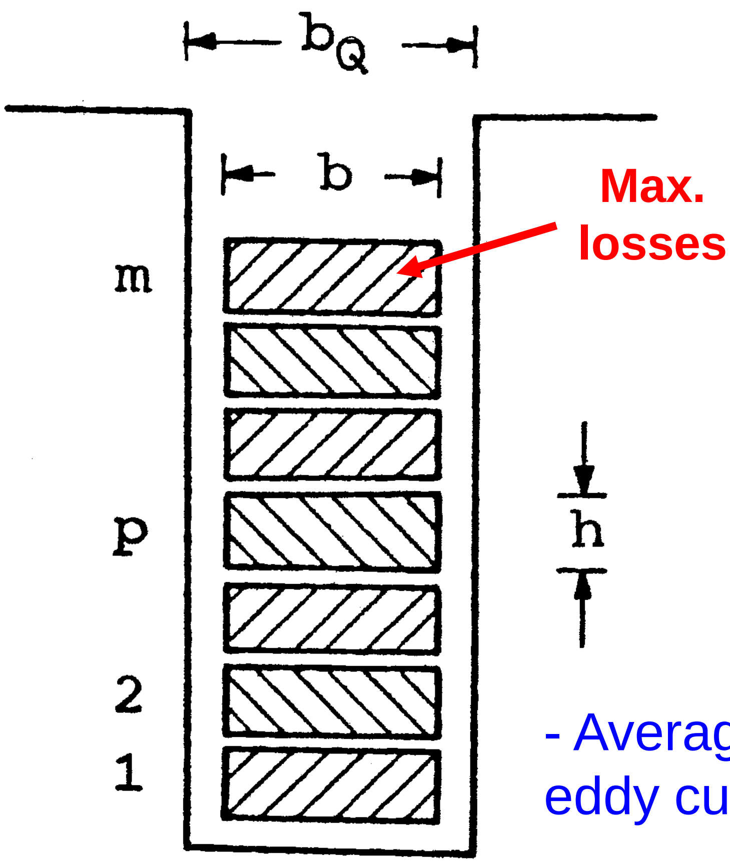
- So its eddy current losses are increased !

- p^{th} turn: $k_{R,p} = \varphi(\xi) + p\cdot(p-1)\cdot\psi(\xi)$

- Eddy current losses in massive conductors are called 2^{nd} order losses !

Source: Neidhöfer, G., BBC, Switzerland

Field´s equation for 2nd order eddy current losses



Source: Neidhöfer, G., BBC, Switzerland

- Increase of losses in p^{th} turn due to eddy currents:

$$\boxed{k_p = \varphi(\xi) + p(p-1)\psi(\xi)}$$

$$\varphi(\xi) = \xi \cdot \frac{\sinh 2\xi + \sin 2\xi}{\cosh 2\xi - \cos 2\xi}$$

$$\psi(\xi) = 2\xi \frac{sh\xi - \sin\xi}{ch\xi + \cos\xi}$$

$$\xi = \frac{h}{d_E} = h\sqrt{\pi f \mu \kappa \frac{b}{b_Q}}$$

- Average increase of losses per turn (m turns assumed):

$$\boxed{k_m = \frac{1}{m}\sum_{p=1}^{m} k_p = \varphi(\xi) + \frac{m^2 - 1}{3}\psi(\xi)}$$

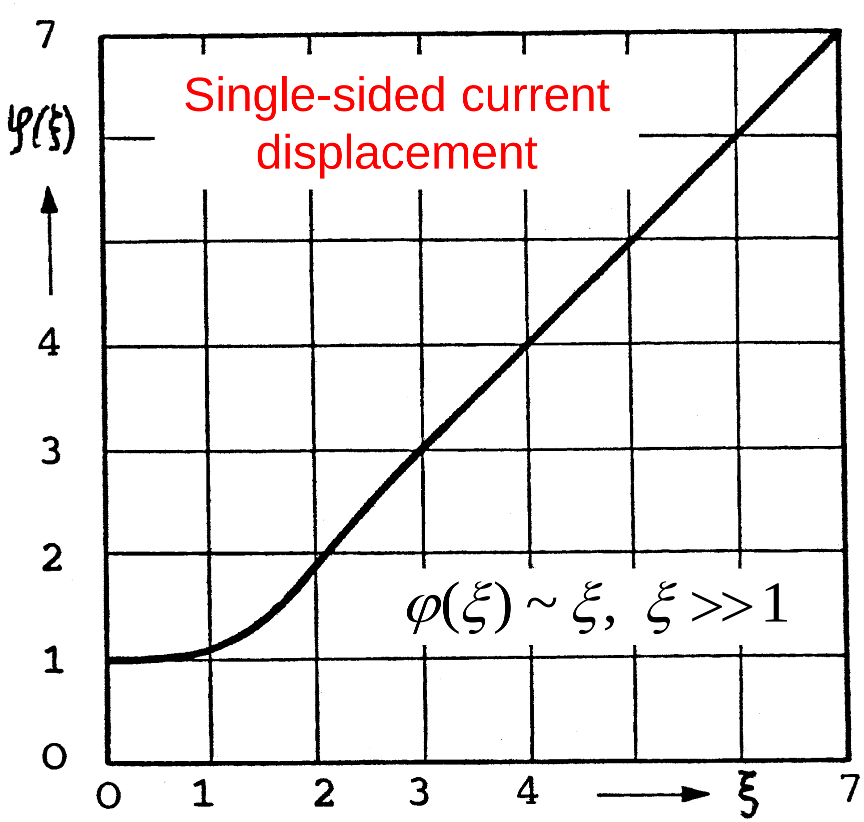
- Average of slot (eddy currents) and winding overhangs (no eddy currents):

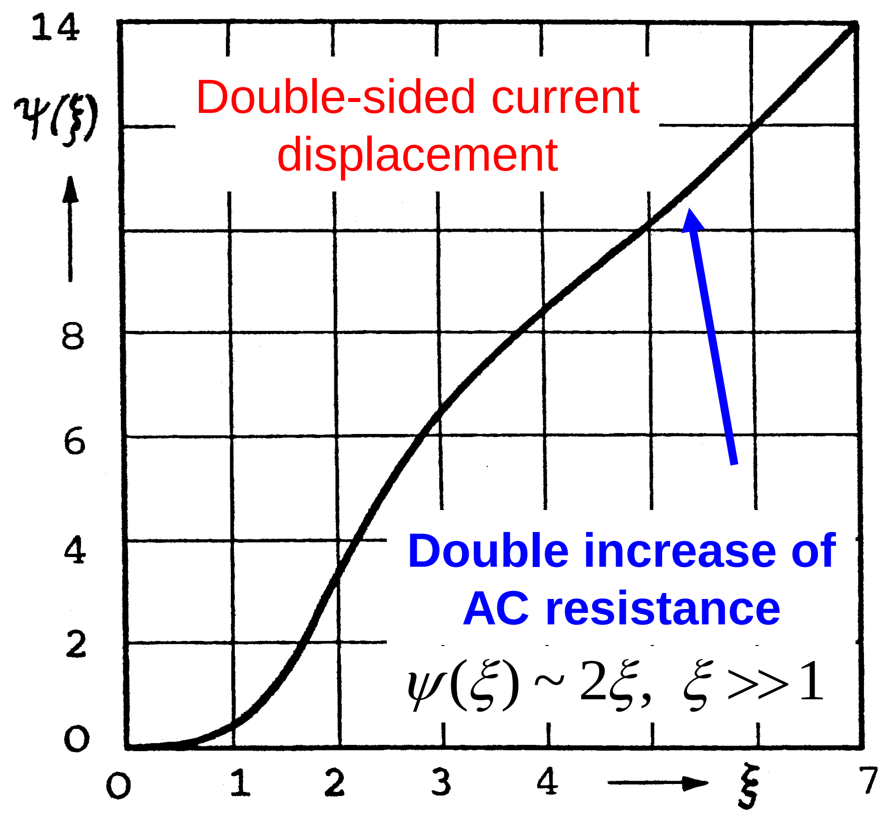
$$\boxed{k_R = \frac{k_m \cdot l_{Fe} + l_b}{l_{Fe} + l_b}}$$

Field´s loss functions (FIELD & EMDE, 1912)

$$\varphi(\xi) = \xi \cdot \frac{\sinh 2\xi + \sin 2\xi}{\cosh 2\xi - \cos 2\xi}$$

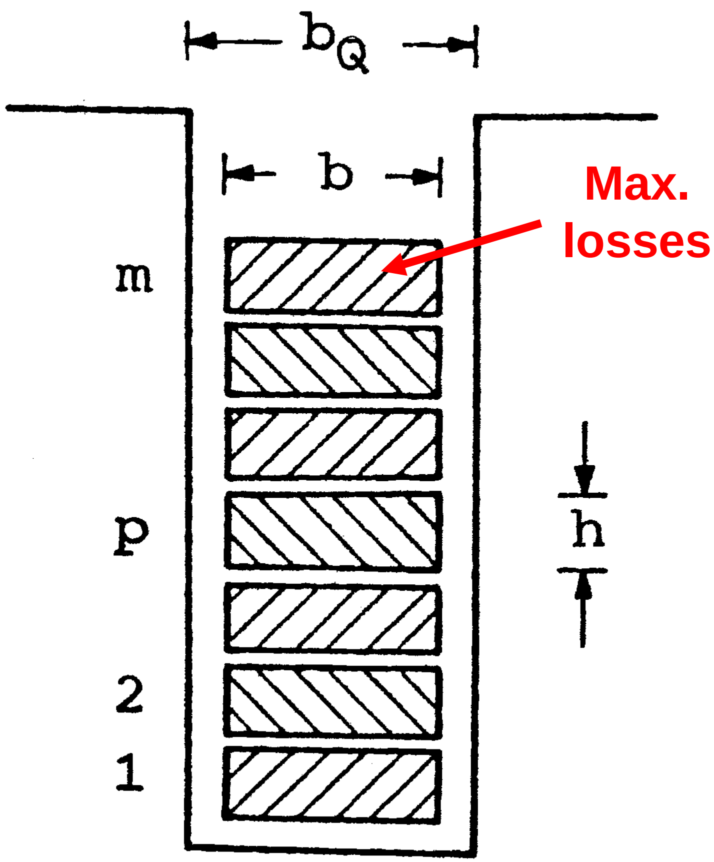
$$\psi(\xi) = 2\xi \frac{sh\xi - \sin\xi}{ch\xi + \cos\xi}$$





Source: Neidhöfer, G., BBC, Switzerland

Field´s formula for 2nd order eddy current losses



- Number m:

Single layer winding: $m = N_c$ is number of turns per coil

Two-layer winding: $m = 2N_c$ is TWICE number of turns per coil

- Loss increase in top conductor $p = m$:

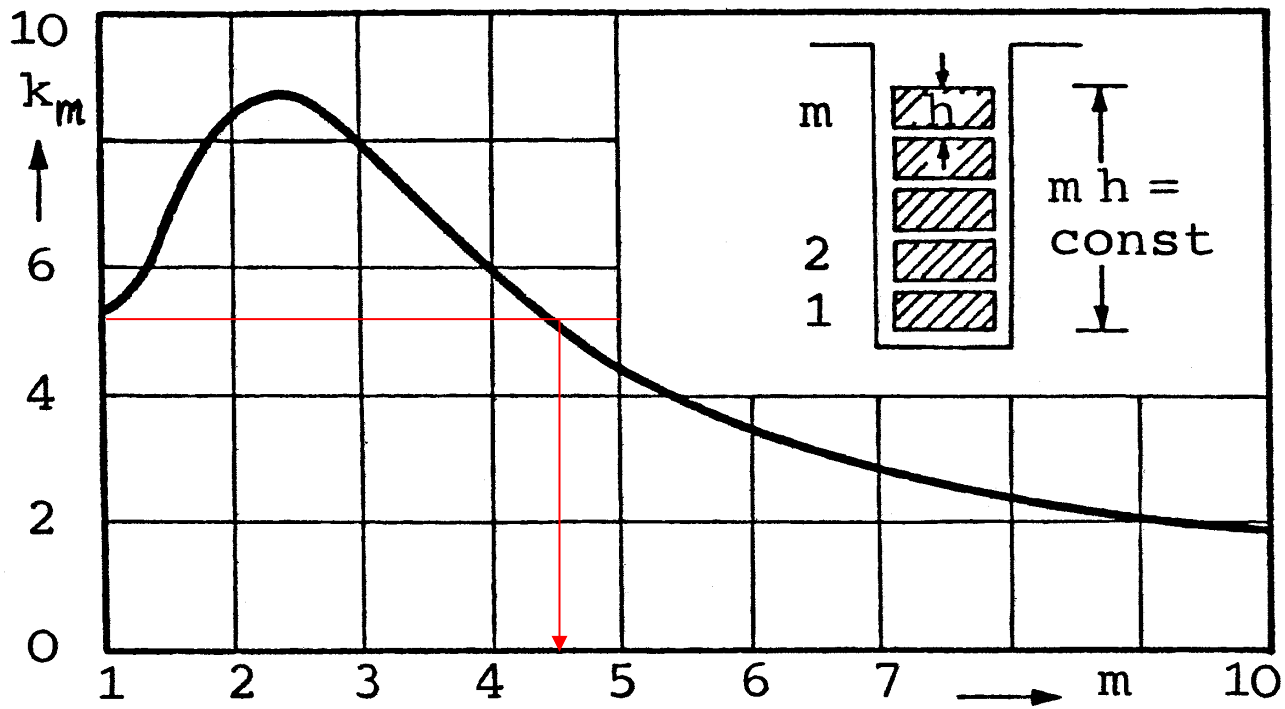
$$\boxed{k_{p=m} = \varphi(\xi) + m(m-1)\psi(\xi)}$$

Top conductor suffers maximum additional losses due to eddy currents !

Source: Neidhöfer, G., BBC, Switzerland

2^{nd} order losses with increased number of turns *m*

Example: b/b_Q = 0.8, 50 Hz
Total slot height $m \cdot h$ = 60 mm = constant, but m increases !
Is k_m increasing / decreasing, as conductor height h = 60mm/m decreases ?



- Eddy current losses increase from one conductor to two conductors per slot !

- The average losses per conductor k_m/m decrease at constant current density J !

Source: Neidhöfer, G., BBC, Switzerland

3. Eddy current losses in winding systems

Reduction of 2nd order losses (1)

- Increase number of turns per slot to reduce conductor height *h*:

Aim: $$\xi = \frac{h}{d_E} = h\sqrt{\pi f \mu \kappa \frac{b}{b_Q}} < 0.3$$

- *Example:* 12-pole synchronous generator: $n = 500/\text{min}$, $2p = 12$, $f = 50\ \text{Hz}$

- Stator winding: $N_c = 2$, $q = 2$, $W = 5/6\,\tau_p$, $a = 2$, $\tau_p = 0.5\ \text{m}$, $l = 1\ \text{m}$, $m = 2N_c = 2\text{x}2 = 4$

- Number of turns per phase: $N = 2pqN_c / a = 12\cdot 2\cdot 2/2 = \underline{\underline{24}}$

If number of parallel winding branches per phase *a* is increased,

- the number of turns per slot N_c increases,

- the current per winding branch $I_c = I_s/a$ decreases and so does *h*.

- $a = 6$ instead of 2: $m = 2N_c = 12$ is tripled, *h* is one third of old value

$$N = 2pqN_c / a = 12\cdot 2\cdot 6/6 = \underline{\underline{24}}$$

Result: 2nd order additional losses decreases to about 30% !

Reduction of 2nd order losses (2)

Example: 12-pole synchronous generator: n = 500/min, 2p = 12, f =50 Hz

- Stator winding:

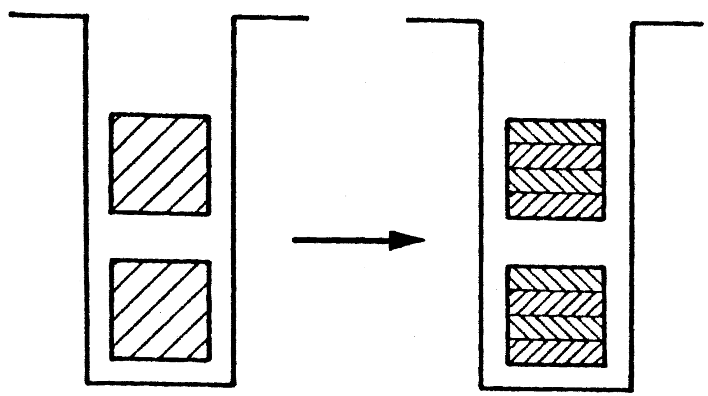
a) $N_c = 1$, $q = 2$, $W = 5/6\,\tau_p$, $a = 1$, $\tau_p = 0.5$ m, $l = 1$ m, $m = 2N_c = 2\text{x}1 = 2$

- Number of turns per phase: $$N = 2pqN_c / a = 12 \cdot 2 \cdot 1/1 = \underline{\underline{24}}$$

b) $N_c = 4$, $q = 2$, $W = 5/6\,\tau_p$, $a = 4$, $\tau_p = 0.5$ m, $l = 1$ m, $m = 2N_c = 2\text{x}4 = 8$

- Number of turns per phase: $$N = 2pqN_c / a = 12 \cdot 2 \cdot 4/4 = \underline{\underline{24}}$$

Result: 2nd order additional losses decreases to about 25% !



Source: Neidhöfer, G., BBC, Switzerland

3. Eddy current losses in winding systems

Critical conductor height for coils $N_c > 1$ (1)

- For $\xi < 1$: *Taylor*-series: $\varphi(\xi) \approx 1 + \frac{4}{45}\xi^4 \qquad \psi(\xi) \approx \frac{\xi^4}{3}$

$$k_m \approx 1 + \frac{4}{45}\cdot\xi^4 + \frac{m^2-1}{3}\cdot\frac{\xi^4}{3} = 1 + \frac{m^2-0.2}{9}\cdot\xi^4$$

- Constant current per conductor *I* , constant number of conductors per slot *m* :

Total losses (with $h = \xi \cdot d_E$): $P_1 = k_m \cdot P_0 = \frac{I^2 L}{b\cdot h\cdot\kappa}\cdot k_m \approx \frac{I^2 L}{b\cdot d_E\cdot\kappa}\cdot\left(\frac{1}{\xi} + \frac{m^2-0.2}{9}\cdot\xi^3\right)$

- Loss **minimum** at $dP_1/d\xi = 0$: $\boxed{\xi_{crit} = \frac{h_{crit}}{d_E} \approx \sqrt[4]{\frac{3}{m^2-0.2}} \approx \sqrt[4]{\frac{3}{m^2}} = \frac{1.32}{\sqrt{m}}}$

- **Optimum increase of 2nd order current displacement losses:**

$$k_{m,opt} = k_m(\xi_{crit}) \approx 1 + \frac{m^2-0.2}{9}\cdot\xi_{crit}^4 \approx 1 + \frac{m^2-0.2}{9}\cdot\frac{3}{m^2-0.2} = 1 + \frac{1}{3} = \underline{\underline{1.33}}$$

Critical conductor height for coils $N_c > 1$ (2)

- Critical conductor height h_{crit} depends on number of conductors m per slot one above the other:

$$\boxed{\xi_{crit} = \frac{h_{crit}}{d_E} = \frac{1.32}{\sqrt{m}}}$$

- Height h_{crit} is smaller, the bigger m is !

Critical total slot height H_{krit} : $$H_{crit} = m \cdot h_{crit} \approx m \cdot d_E \cdot \frac{1.32}{\sqrt{m}} = 1.32 \cdot \sqrt{m} \cdot d_E$$

Facit:

As total critical slot height rises with number m, the total amount of copper height may be increased !

Applicable for “small” machines with high voltage U:

“Small” machine: Flux per pole Φ is small: So need for high N_s and N_c !

High N_c = high m !

$$U \cong \omega \cdot k_w N_s \cdot \Phi$$

3. Eddy current losses in winding systems

Bar winding : $N_c = 1$

- Big generators: Flux per pole Φ is big, so N_s is low: $U \cong \omega \cdot k_w N_s \cdot \Phi$

Often $N_c = 1$, especially with two-pole turbine generators, as maximum number of parallel paths is $a = 2$.

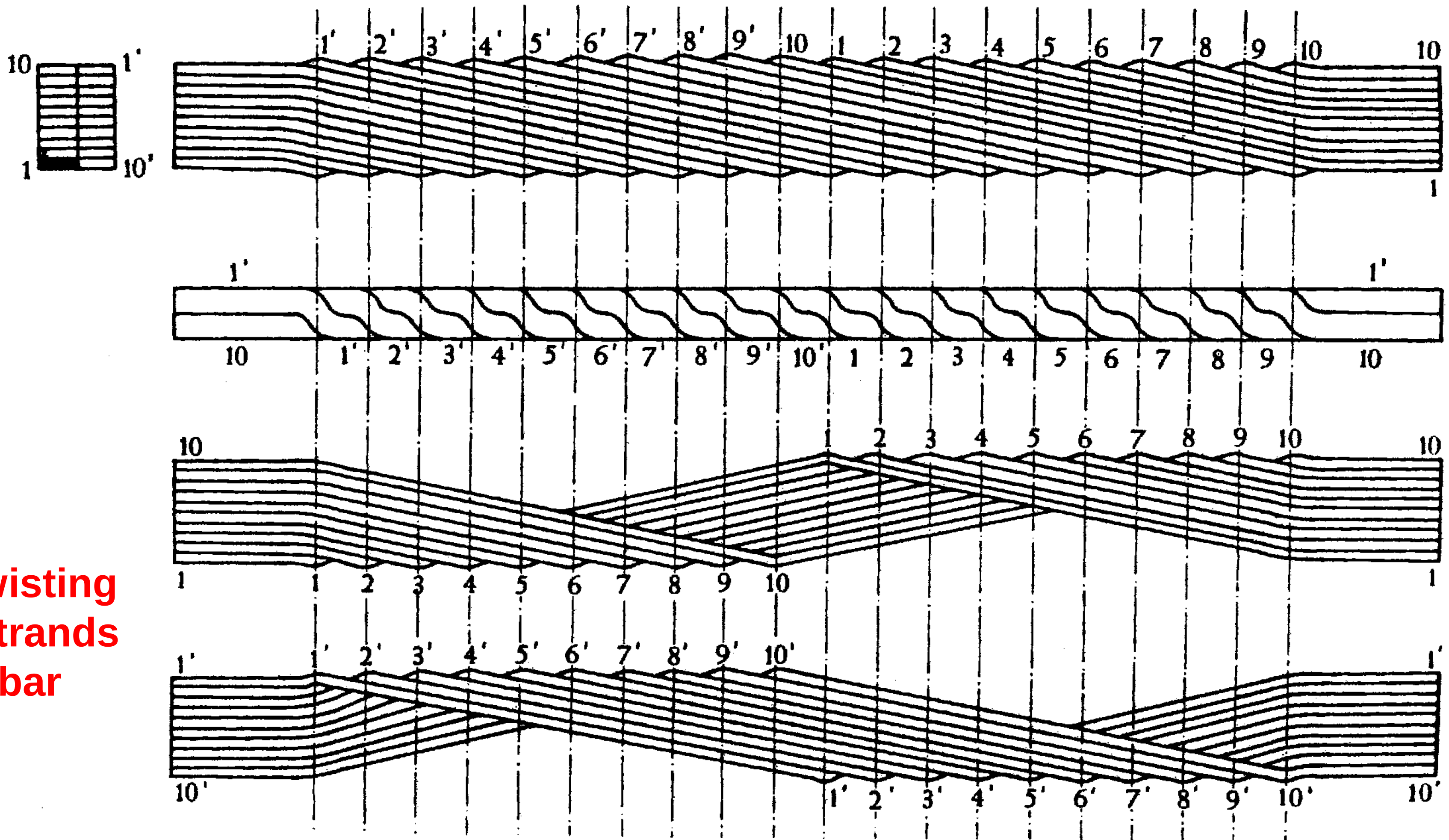
- Partition of bar into small parallel connected conductors leads to big 1st order eddy currents, so twisting of these parallel conductors is necessary to eliminate slot stray flux linkage.

- Patent of *Ludwig Roebel* (German engineer, at *BBC company*): Twisting of profile copper conductors in rectangular slot eliminates 1st order eddy currents.

- In *Roebel*-bars only 2nd order eddy currents remain !

3. Eddy current losses in winding systems

Roebel bar = 20 parallel twisted conductors (strands)

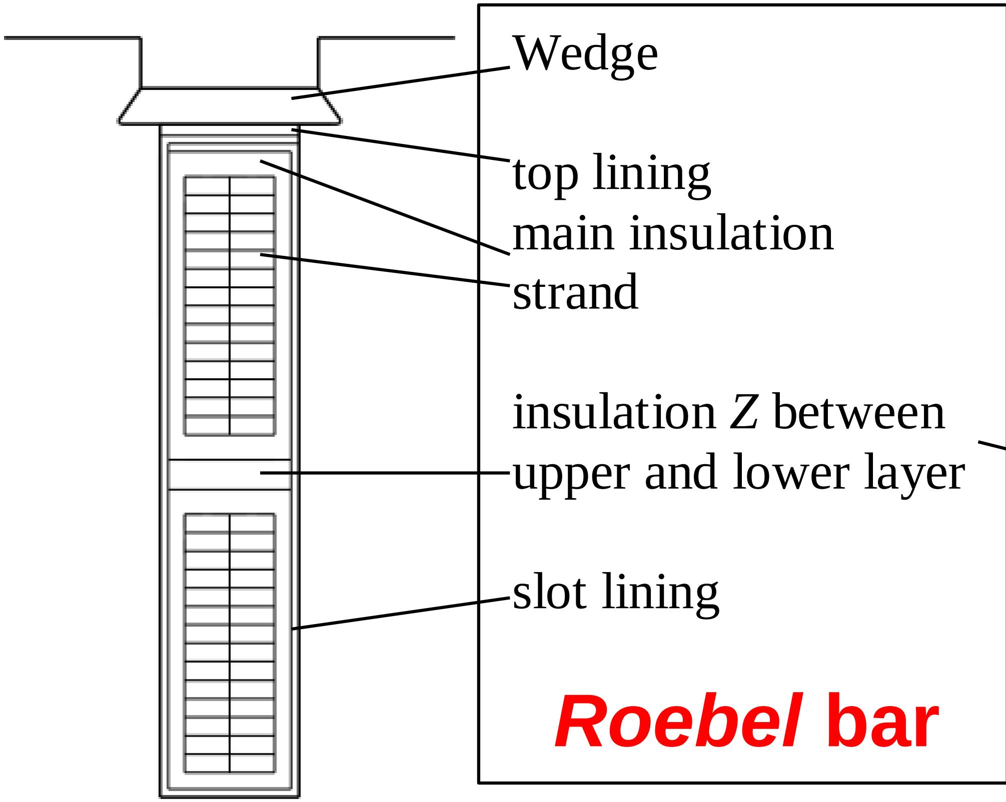


360° twisting of 20 strands per bar

Source: Roebel, L., Deutsches Reichspatent, reprint

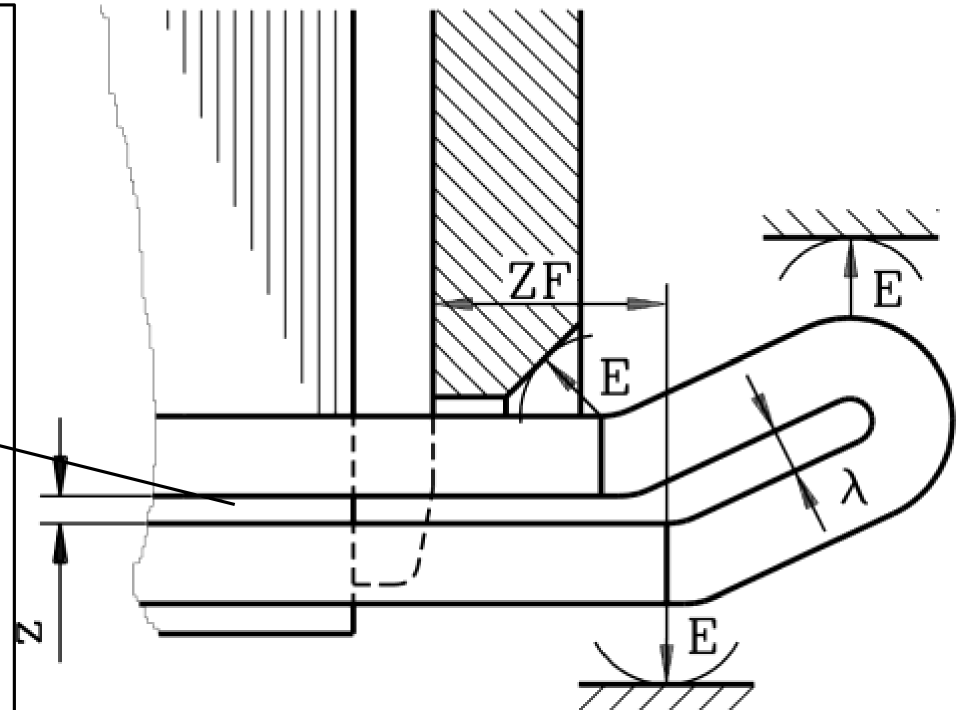
3. Eddy current losses in winding systems

Roebel bar cross section and winding overhang



$N_c = 1$

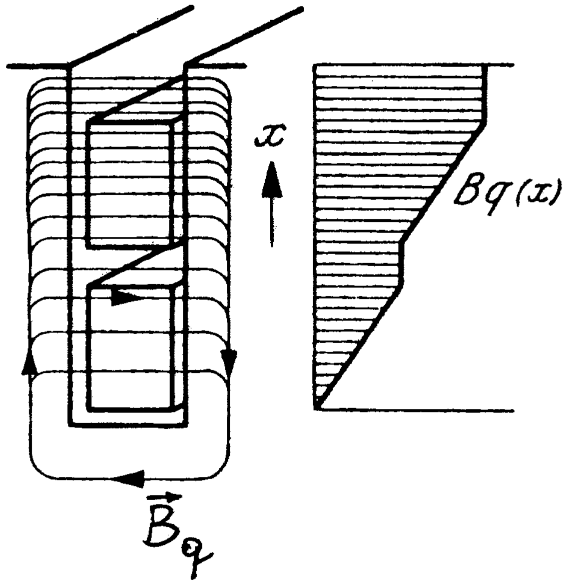
Cross section in slot with 24 strands per bar

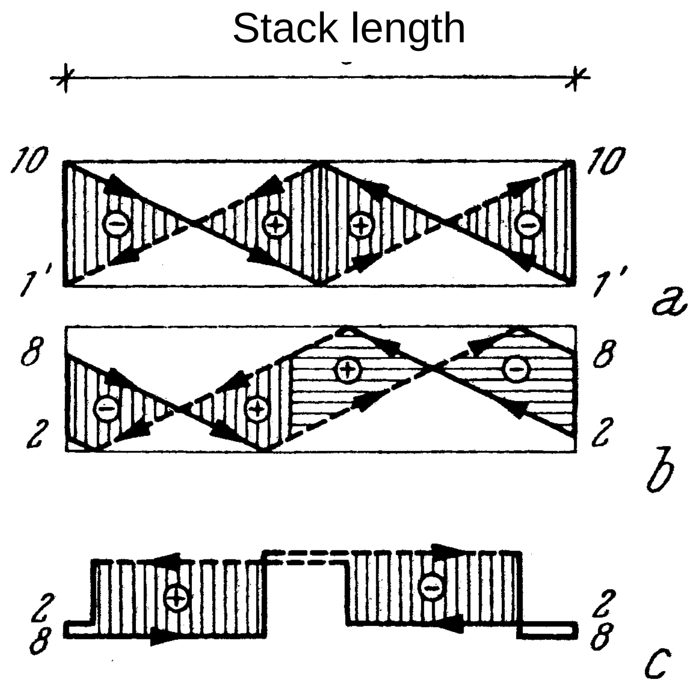


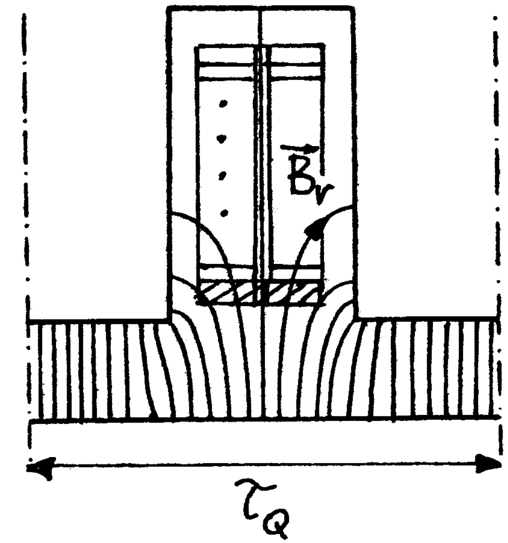
Winding overhang with clearing *E* to end shields (on earth potential) and clearing *ZF* of end of main insulation from pressing construction of iron stack end

3. Eddy current losses in winding systems

Slot stray flux linkage elimination in *Roebel* bars







Source: Neidhöfer, G., BBC, Switzerland

- a), b) Each arbitrarily chosen pair of parallel strands (e.g. 1 and 10, 2 and 8, ...) forms loops, where **positive and negative oriented areas have the same shape and relative position !** So the linkage of linear increasing slot flux density B_q is cancelled completely for each pair !

- c) The radial slot flux B_r of main field experiences likewise for each arbitrarily chosen pair of parallel strands (e.g. 1 and 10, 2 and 8, ...) loops with **positive and negative oriented equal areas:** So also radial flux linkage is cancelled completely for each pair of strands !

3. Eddy current losses in winding systems

Example:

ROEBEL-bars: 2x12 strands: strand geometry h_T = 2 mm, f = 60 Hz, ϑ_{Cu} = 100 °C, b/b_Q = 0.7, winding overhang length ratio: l_b/l_{Fe} = 0.65.

$$\xi = \frac{h_T}{d_E} = h_T \sqrt{\pi f \mu_0 \kappa \frac{b}{b_Q}} = 0.002\sqrt{\pi \cdot 60 \cdot 4\pi 10^{-7} \cdot 43.4 \cdot 10^6 \cdot 0.7} = 0.17$$

m = 24 strands one above the other ! 2nd order eddy current losses:

FIELD´s formulas: $\varphi(\xi) \approx 1 + \frac{4}{45}\xi^4 = 1.000074$, $\psi(\xi) \approx \frac{\xi^4}{3} = 0.000276$

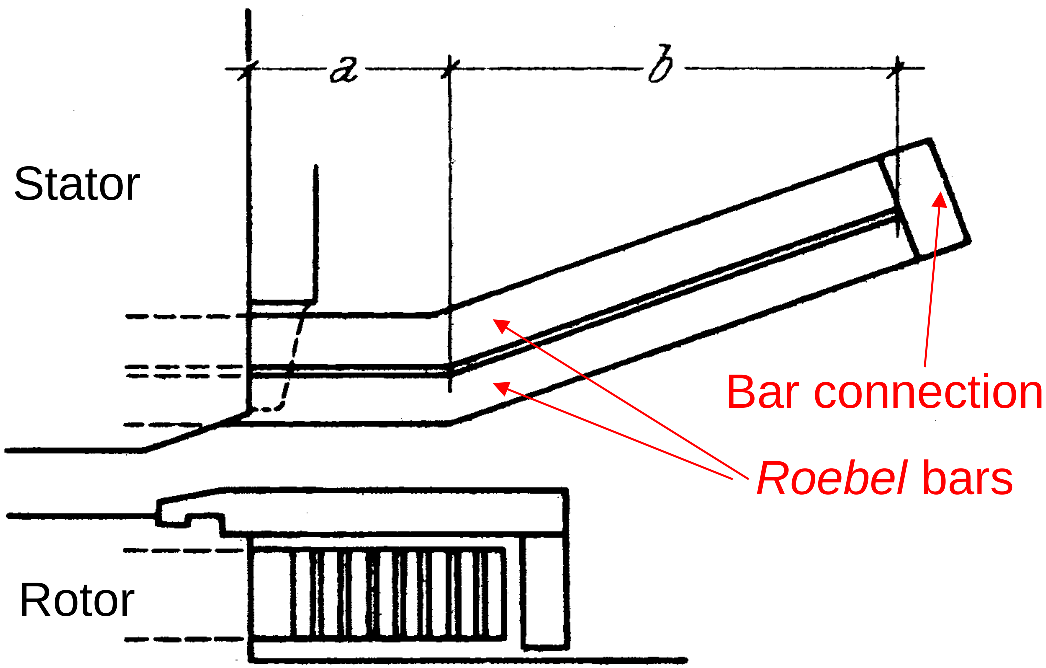
$$k_m = \varphi(\xi) + \frac{m^2 - 1}{3}\psi(\xi) = 1.000074 + \frac{24^2 - 1}{3} \cdot 0.000276 = 1.000074 + 0.053 = \underline{\underline{1.0531}}$$

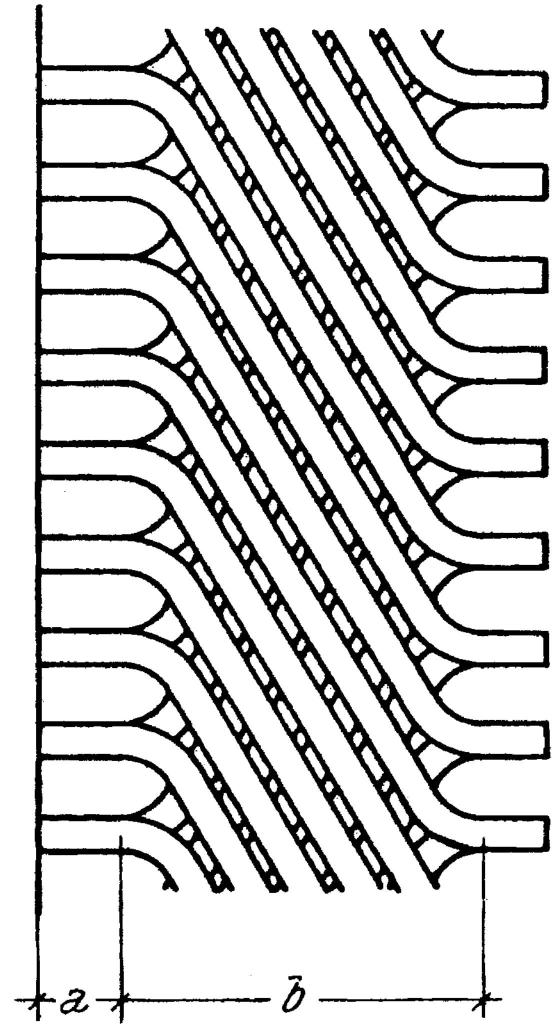
Average value per turn: $k_R = \frac{k_m + (l_b / l_{Fe})}{1 + (l_b / l_{Fe})} = \frac{1.0531 + 0.65}{1.65} = \underline{\underline{1.032}}$

Average increase of losses is only 3.2%. No 1st order eddy current occur !

3. Eddy current losses in winding systems

Winding overhang geometry with *Roebel* bars





Winding overhang geometry of a two-layer winding of a turbine generator with *Roebel* bars

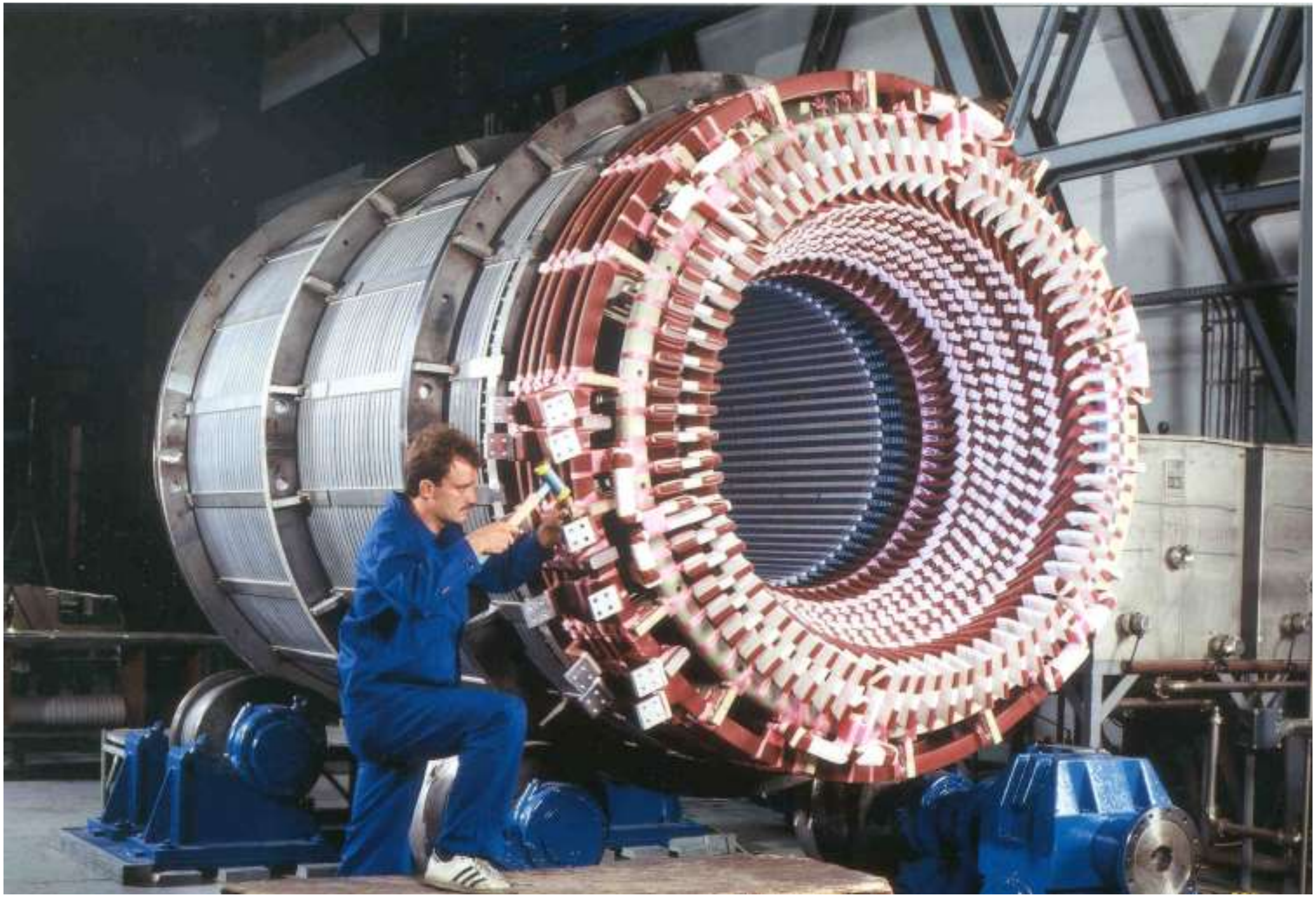
- (a): straight part of overhang
- (b): curved part of overhang

Source: Sequenz, H. (Ed.), Springer-Verlag

3. Eddy current losses in winding systems

Winding overhang geometry with *Roebel* bars

Air-cooled 2-pole turbine generator



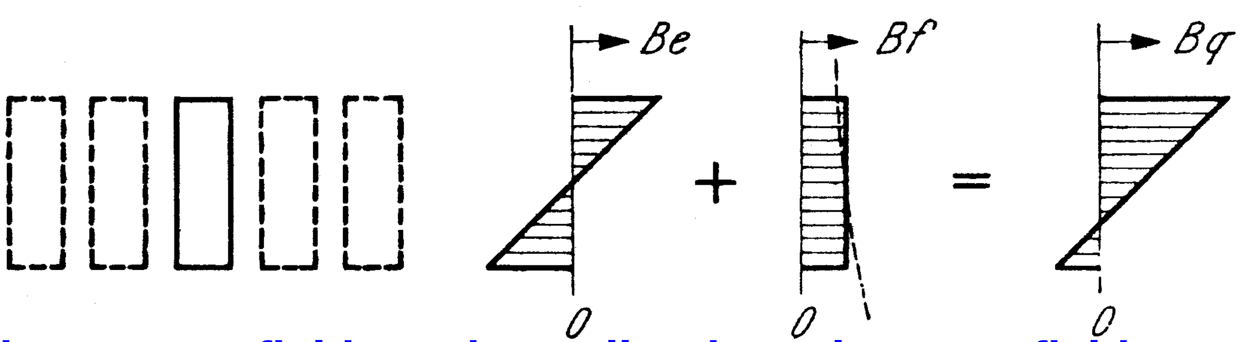
Source:

BBC (now Alstom), Switzerland

3. Eddy current losses in winding systems
Winding overhang stray flux in *Roebel* bars

Source: Sequenz, H. (Ed.), Springer-Verlag

One layer of bars in section (a)



- Winding overhang stray field much smaller than slot stray field, so twisting of winding overhang in hydro generators not done !

Note: Low speed = high pole count = small pole pitch = short winding overhang: eddy current losses in winding overhang of minor importance ! But in two-pole turbine generators: LONG winding overhangs, so transposition of strands is NECESSARY !

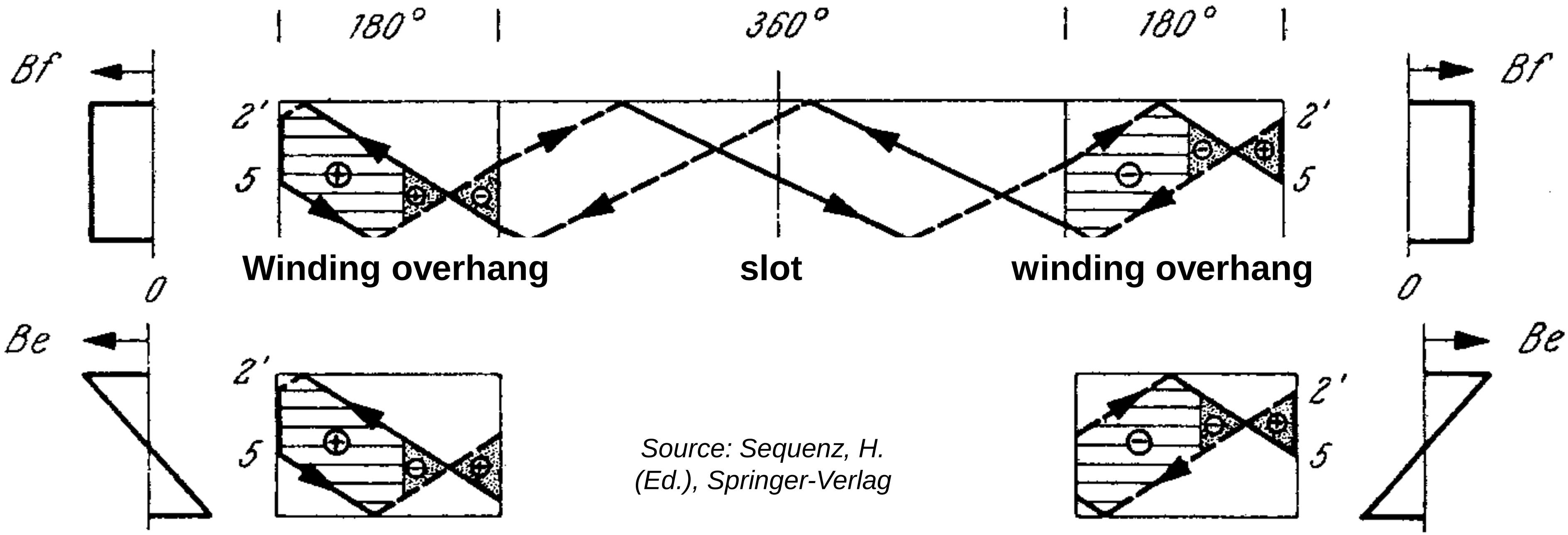
- Cross section of bars e.g. in section (a): *Transversal component of stray field B_q:*

B_e: Self field of on bar in bar axis B_f: External field of bars of other layer in bar axis

- Condition for elimination 1st order eddy currents in winding overhangs:

Twisting of strands in winding overhang must eliminate stray flux linkage of resulting transversal stray field B_q (=sum of B_e and B_f), hence of self field AND of external field !

Winding overhang stray flux linkage elimination in *Roebel* bars (1)



Source: Sequenz, H. (Ed.), Springer-Verlag

Example: 180° twisting of strands in winding overhangs **(180°/360°/180°):**

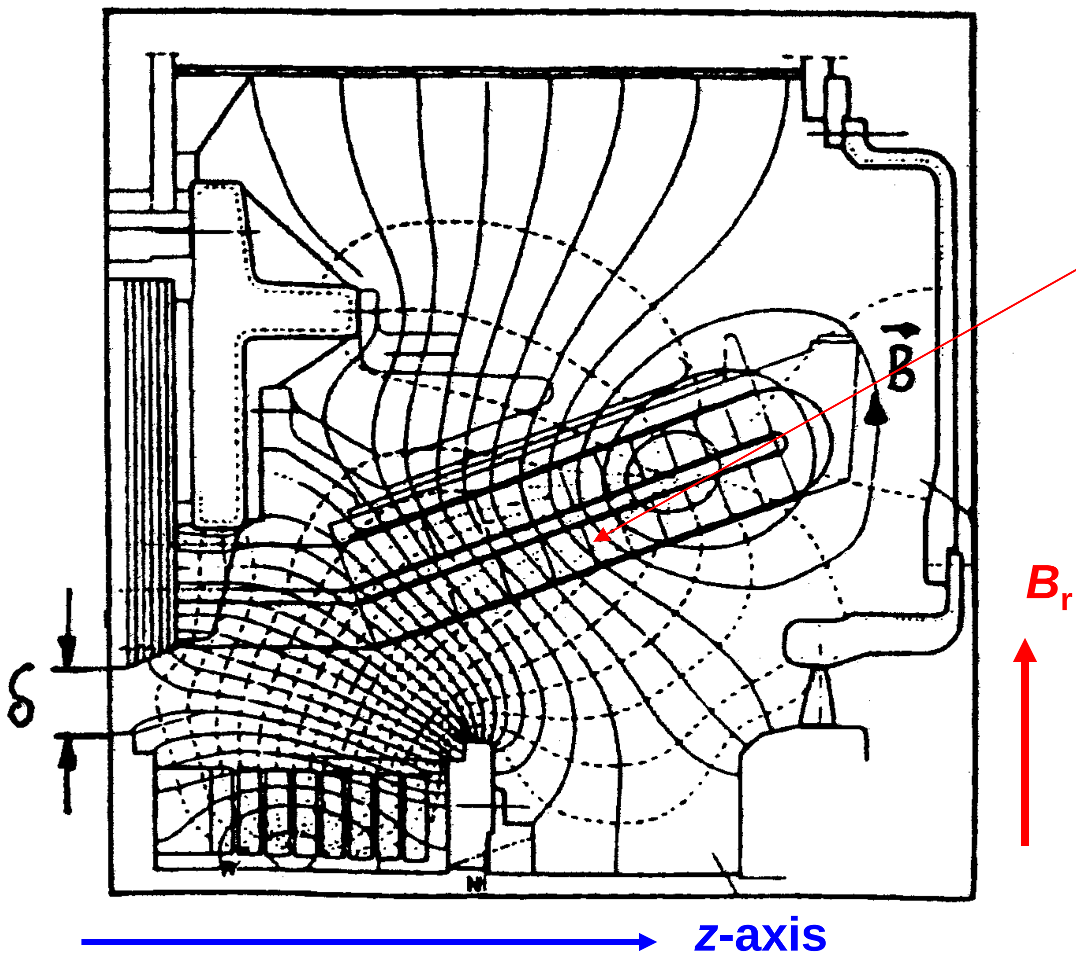
- Each arbitrarily chosen pair of parallel strands (e.g. 2 and 5, ...) forms loops, where **positive and negative oriented areas have the same shape and relative position !** So

  - the linkage of linear changing self-field flux density B_e and

  - the linkage of the (more or less constant) external flux density B_f is cancelled **completely for each pair !**

3. Eddy current losses in winding systems

Stray field in winding overhang under load



- Winding overhang of stator experiences also strong radial stray field component B_r, which has to be taken into account for stray losses in very big machines

- In smaller machines it may be neglected, as the stray flux linkage area for radial field B_r is much smaller than for transverse field B_q !

- E.g. section (a): Length L_a:

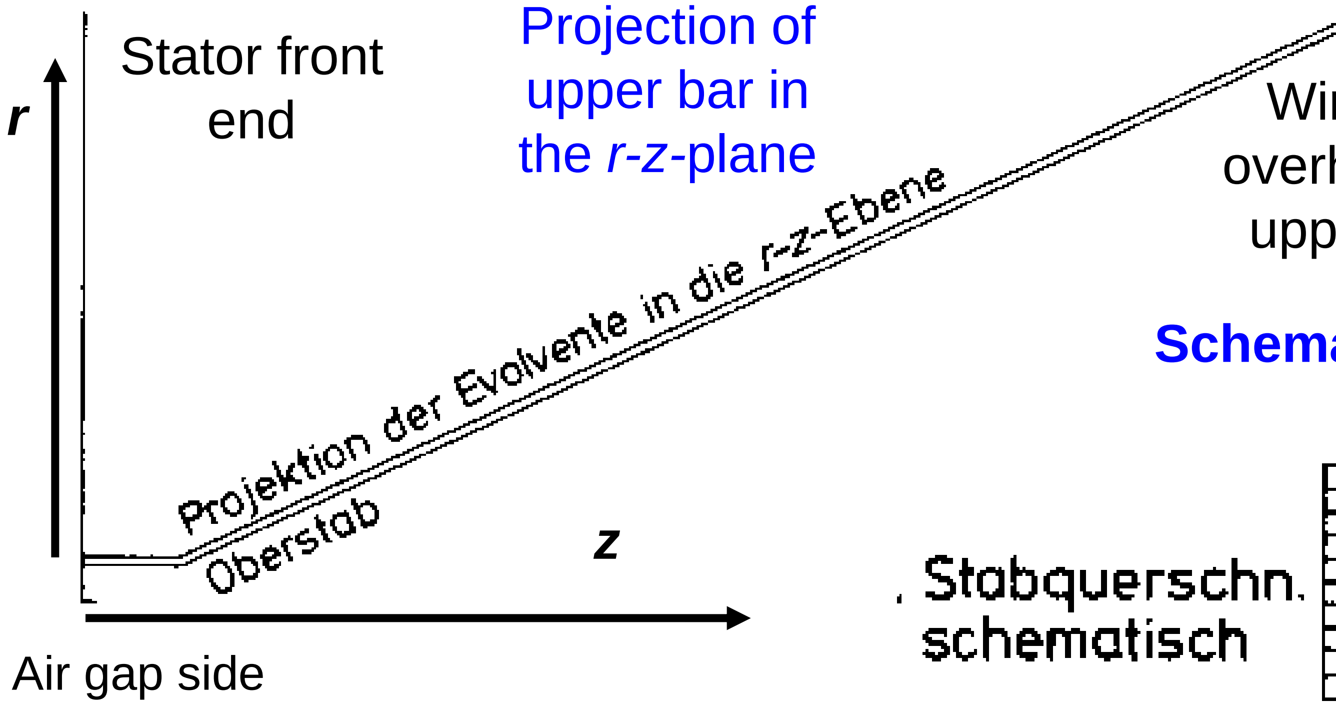
Area for B_r : $2 x b_L x L_a$

Area for B_q : $(m/2) x h_L x L_a$

Source: Darrieux, G., BBC, Switzerland

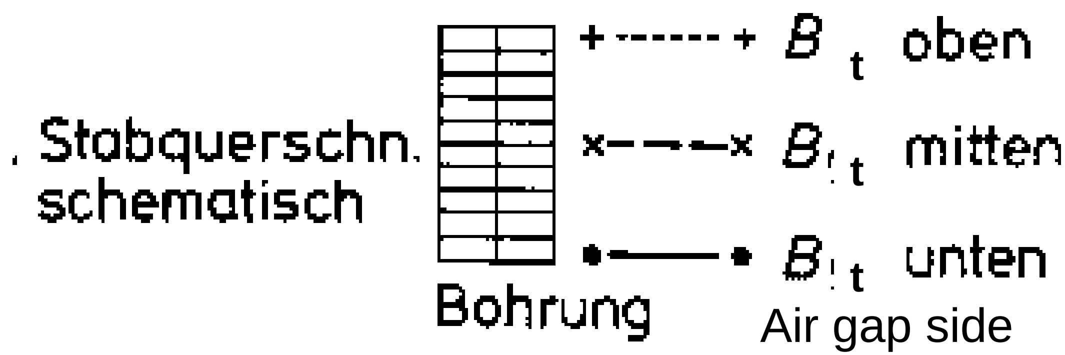
3. Eddy current losses in winding systems

Model for numerical calculation of tangential flux density component along the upper bar in the winding overhang in axial direction (superconducting turbine generator, 3 GVA, rated load)

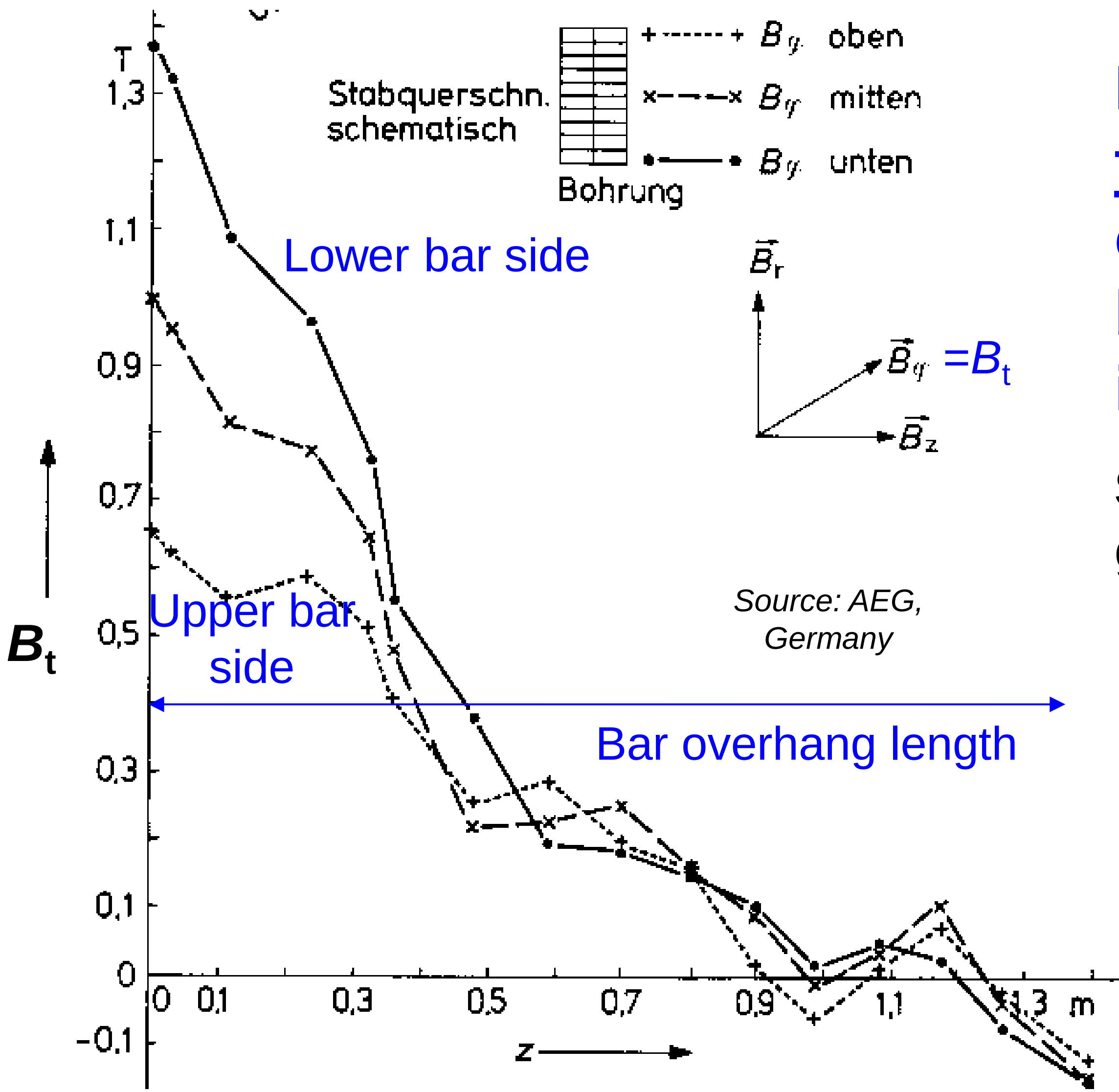


Source: AEG, Germany

Schematic cross section of upper bar



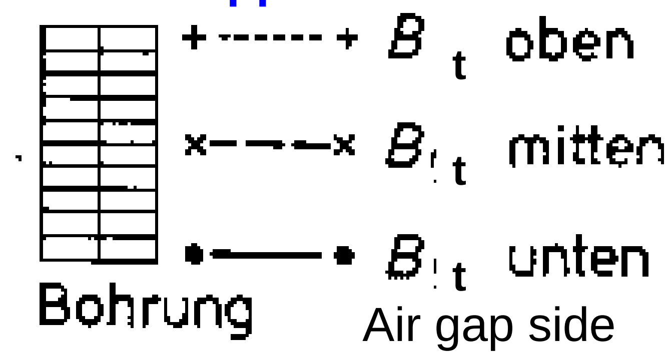
3. Eddy current losses in winding systems



Numerically calculated <u>tangential</u> flux density component along the upper bar in the winding overhang in axial direction

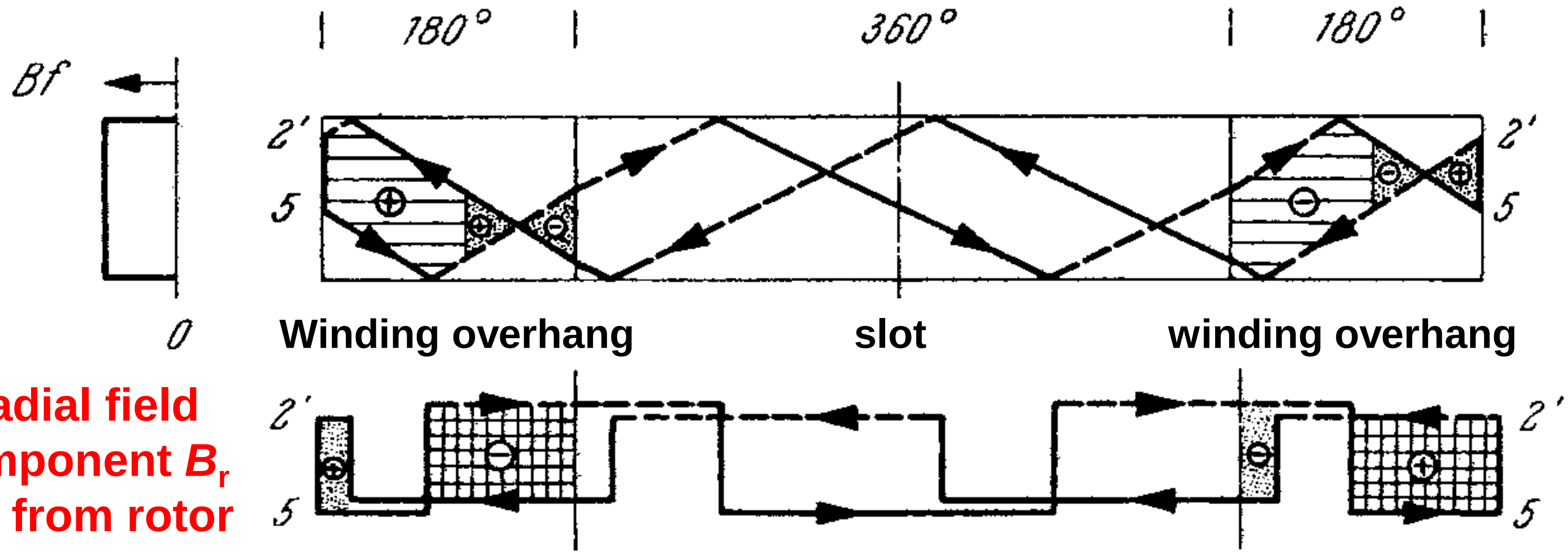
Superconducting turbine generator, 3 GVA, rated load

Schematic cross section of upper bar



3. Eddy current losses in winding systems

Winding overhang stray flux linkage elimination in *Roebel* bars (2)



Radial field component B_r e.g. from rotor

Source: Sequenz, H. (Ed.), Springer-Verlag

Example: 180° twisting of strands in winding overhangs **(180°/360°/180°):**

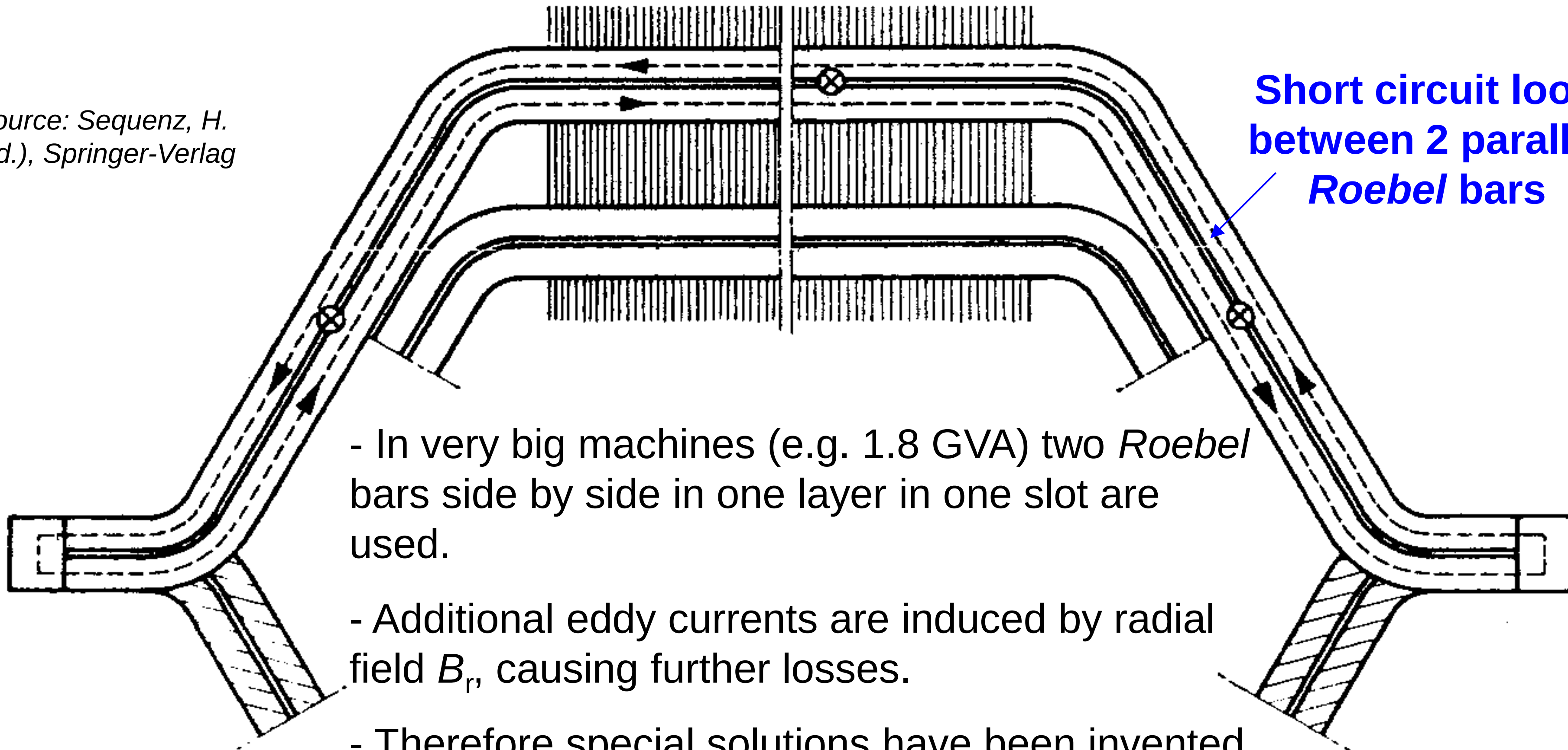
- If B_r **is constant along z-axis, then** its flux linkage is also cancelled ! Usually $B_r(z)$ decreases with increasing distance from iron stack ! So **180°/360°/180°** does not fully cancel radial stray flux linkage !

Note: Special (very expensive) **180°/540°/-180°** eliminates also flux linkage due to $B_r(z)$, which is varying with co-ordinate z !

3. Eddy current losses in winding systems

Parallel connection of 2 *Roebel* bars per slot

Source: Sequenz, H. (Ed.), Springer-Verlag



Short circuit loop between 2 parallel *Roebel* bars

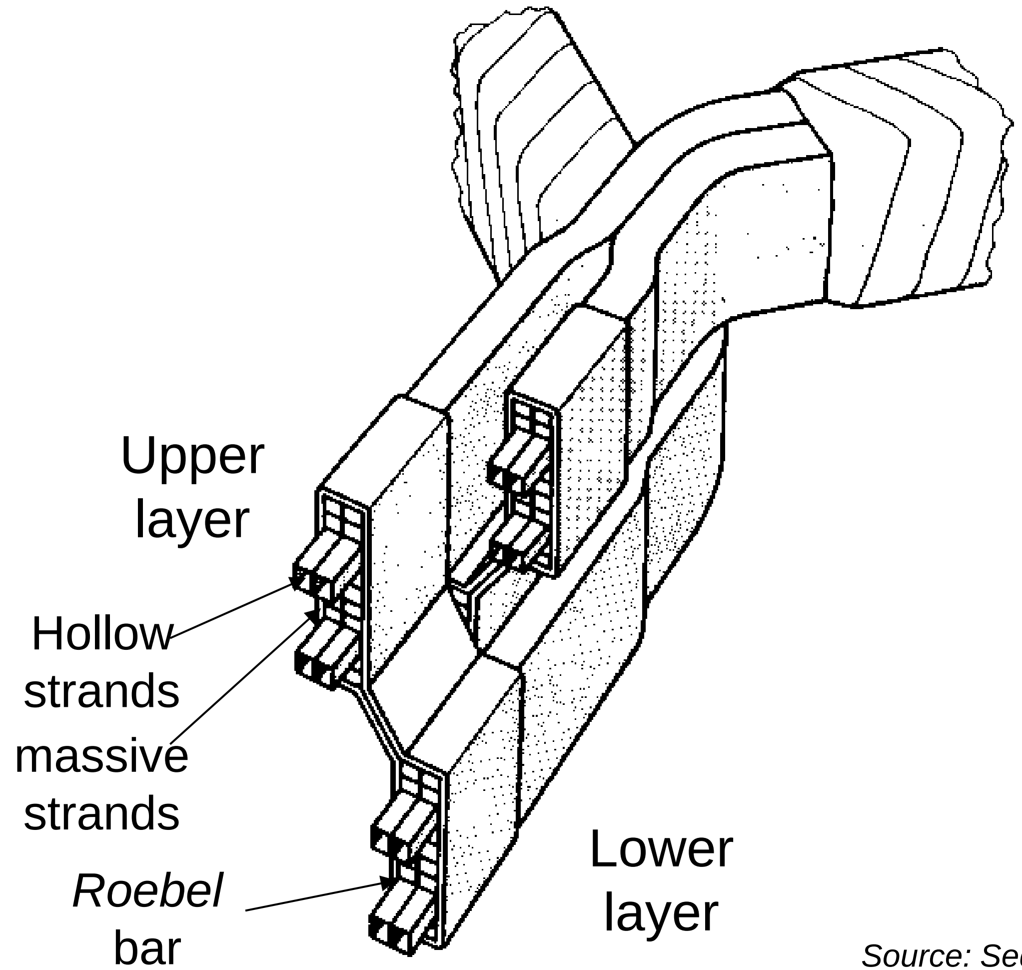
- In very big machines (e.g. 1.8 GVA) two *Roebel* bars side by side in one layer in one slot are used.

- Additional eddy currents are induced by radial field B_r, causing further losses.

- Therefore special solutions have been invented, e.g. transposed parallel connection of *Roebel* bars !

3. Eddy current losses in winding systems

Crosswise connection of 2 parallel *Roebel* bars per slot



-Transposed parallel connection of 2 parallel *Roebel* bars per slot!

- Transposition is done in the winding overhang!

- Transposition leads to a short circuit loop of **four** *Roebel* bars, where the two half loops have opposite flux linkage

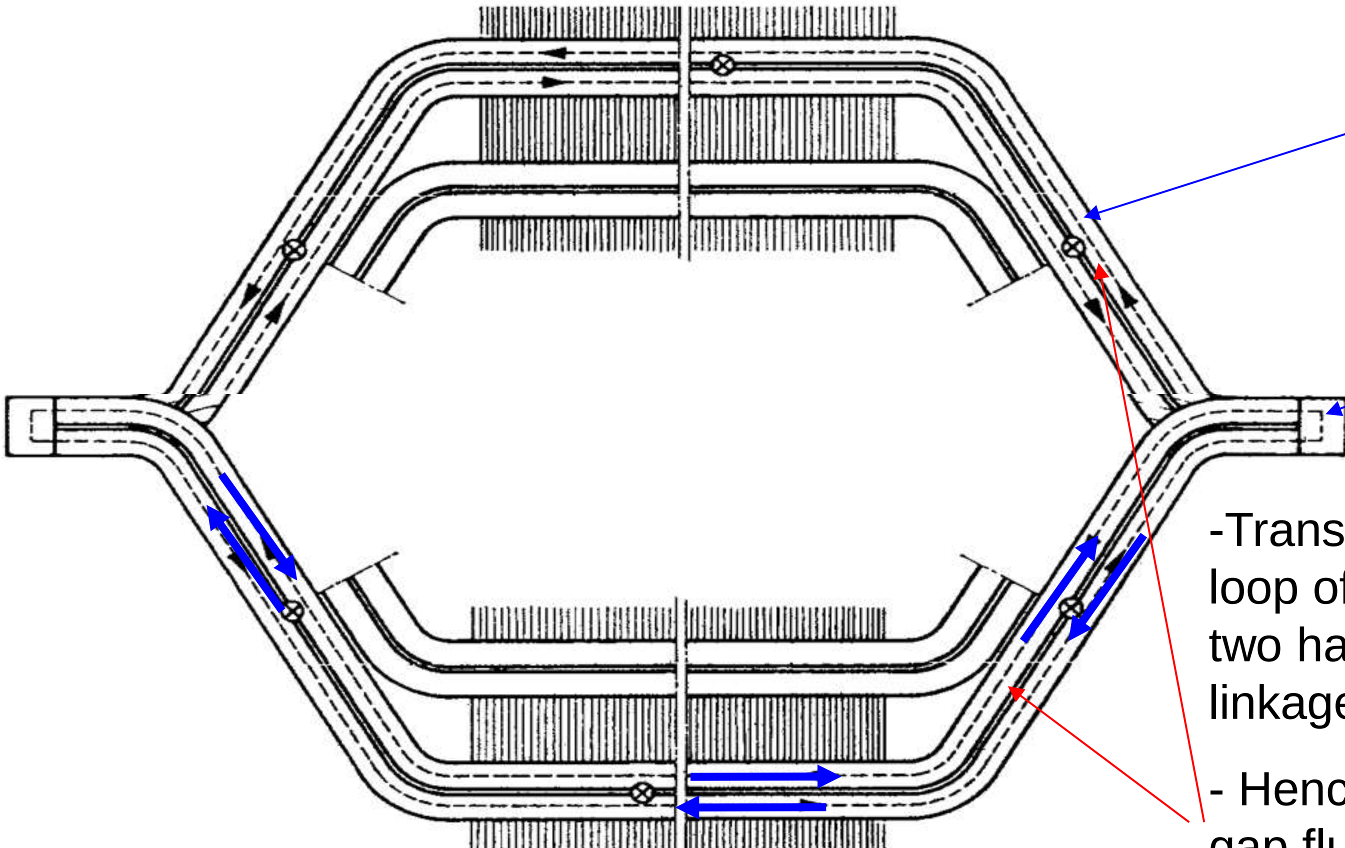
- Hence total flux linkage of radial air gap flux density per short circuit loop is cancelled !

- No additional current induced !

Source: Sequenz, H. (Ed.), Springer-Verlag

3. Eddy current losses in winding systems

Crosswise connection of 2 parallel *Roebel* bars per slot



Source: Sequenz, H. (Ed.), Springer-Verlag

Short circuit loop, built up by 4 *Roebel* bars

Transposition of *Roebel* bars

-Transposition leads to a short circuit loop of **four** *Roebel* bars, where the two half loops have opposite flux linkage

- Hence total flux linkage of radial air gap flux density per short circuit loop is cancelled !

- No additional current induced !

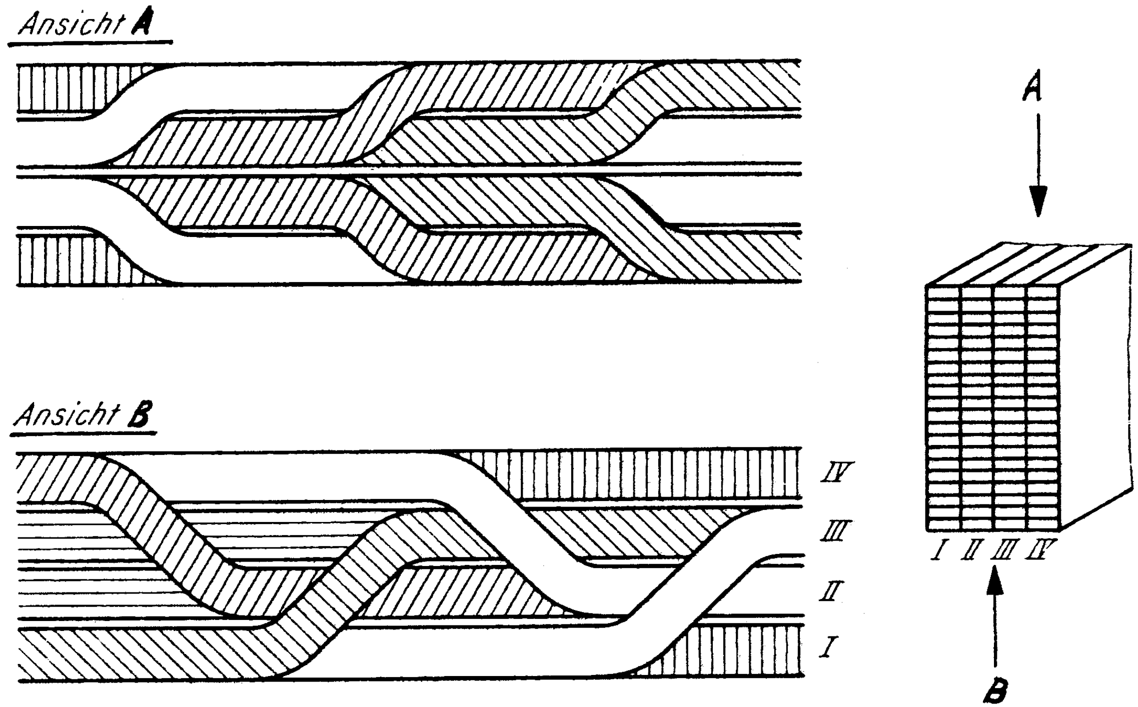
3. Eddy current losses in winding systems

Complete twisting of four rows of strands

View A

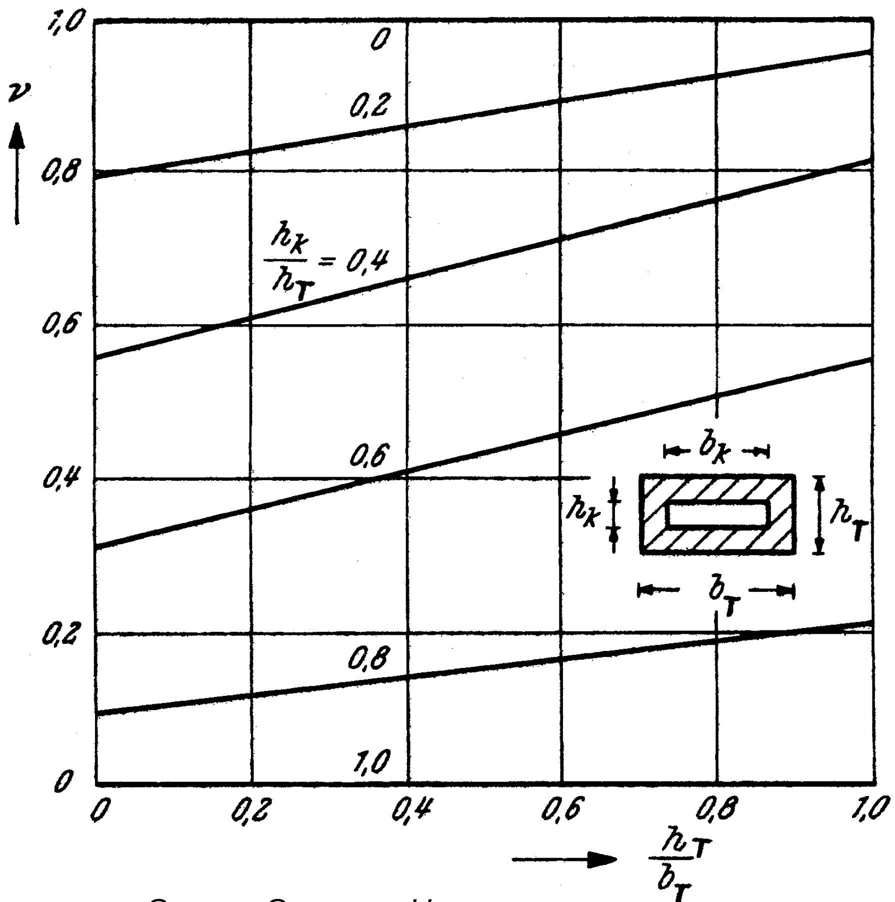
Source: Sequenz, H. (Ed.), Springer-Verlag

View B



- Instead of parallel connection of two *Roebel* bars per slot a complete twisting of four rows of strands (rows I, II, III, IV) is possible, but very expensive, so rarely done !

Eddy current losses in hollow conductors (1)



Source: Sequenz, H. (Ed.), Springer-Verlag

- In *Roebel* bars with included hollow conductors for direct liquid cooling the conductor height h_T is increased due to the duct height h_k !

- But the copper cross section is the same as in massive strands without duct !

- For slot stray flux caused 2nd order eddy currents FIELD´s formulas can be used, if the **hollow conductor coefficient** ν is used :

$$\boxed{k_m = 1 + \frac{m^2 - 0.2}{9}\xi^4 \nu}$$

If ***all*** conductors are hollow !

$$\nu = \frac{12 \cdot J_T \cdot A_T}{b_T^2 h_T^4}$$

$$J_T = \frac{1}{12} \cdot \left(b_T h_T^3 - b_k h_k^3 \right) \qquad A_T = b_T h_T - b_k h_k$$

3. Eddy current losses in winding systems

Eddy current losses in hollow conductors (2)

***Roebel* bar with mixed massive and hollow conductors (strands):**

Two layer winding:

$m_H/2$: numbers of hollow strands in vertical direction per bar

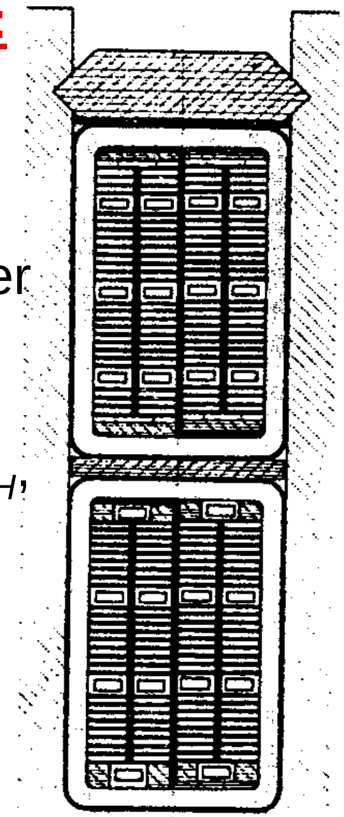
$m_V/2$: number of massive strands in vertical direction per bar

$m/2 = m_H/2 + m_V/2$: total number of strands in vertical direction per bar

Simplified calculation:

Current displacement of massive strands k_{mV} and hollow strands k_{mH}, are regarded separately, as if all strands were hollow or massive:

$$k_{mV} = 1 + \frac{m^2 - 0.2}{9}\xi_V^4 \quad , \quad k_{mH} = 1 + \frac{m^2 - 0.2}{9}\xi_H^4 \nu$$



$m_H = 6$, $m_V = 24$
$m = 30$

Average increase of losses due to eddy currents in all strands:

$$\boxed{k_{m,V+H} = k_{mV}\cdot\frac{m_V}{m} + k_{mH}\cdot\frac{m_H}{m}}$$

Source: Sequenz, H. (Ed.), Springer-Verlag

Summary:

Methods to reduce current displacement effect

- Eddy currents in massive conductors = 2nd order current displacement
- Massive conductor is split into parallel strands: Unequal current distribution in the strands = increased losses = 1st order current displacement
- Strands may be transposed in the winding overhang = twisting = reduction of 1st order current displacement
- 2nd order current displacement in multi-turn coil by FIELD-EMDE formula
- ROEBEL transposition of strands within the slot reduces 1st order current displacement completely
- Big turbine generators: Also ROEBEL transposition in winding overhang to reduce 1st order current displacement there

3. Eddy current losses in winding systems

3. Eddy current losses in winding systems

3.7 Three phase winding for super-conducting generators

- Wires with super-conductors consist of thin twisted super-conducting filaments, embedded in **copper or silver "matrix" conductor** ! In case of quenching (= super-conductor gets normal conducting due to overload) the resistance of the super-conductor material is so big, that the "matrix" must take over the current !

- **Rotor**: DC excitation: Super-conducting winding = no Ohmic losses !

- **Stator:** AC winding: Eddy current losses in "matrix" of the winding would yield too high losses, causing high amount of cooling power (e.g. 30 K above absolute zero !)

So conventional copper is used for AC three-phase stator winding !

- Big rotor excitation allows big air gap field of 1.5 ... 1.8 T, so stator teeth would be strongly saturated. Therefore teeth are omitted, an additional conductors are placed there, fixed by special non-conducting cylinder of glass fibre ("air gap winding")!

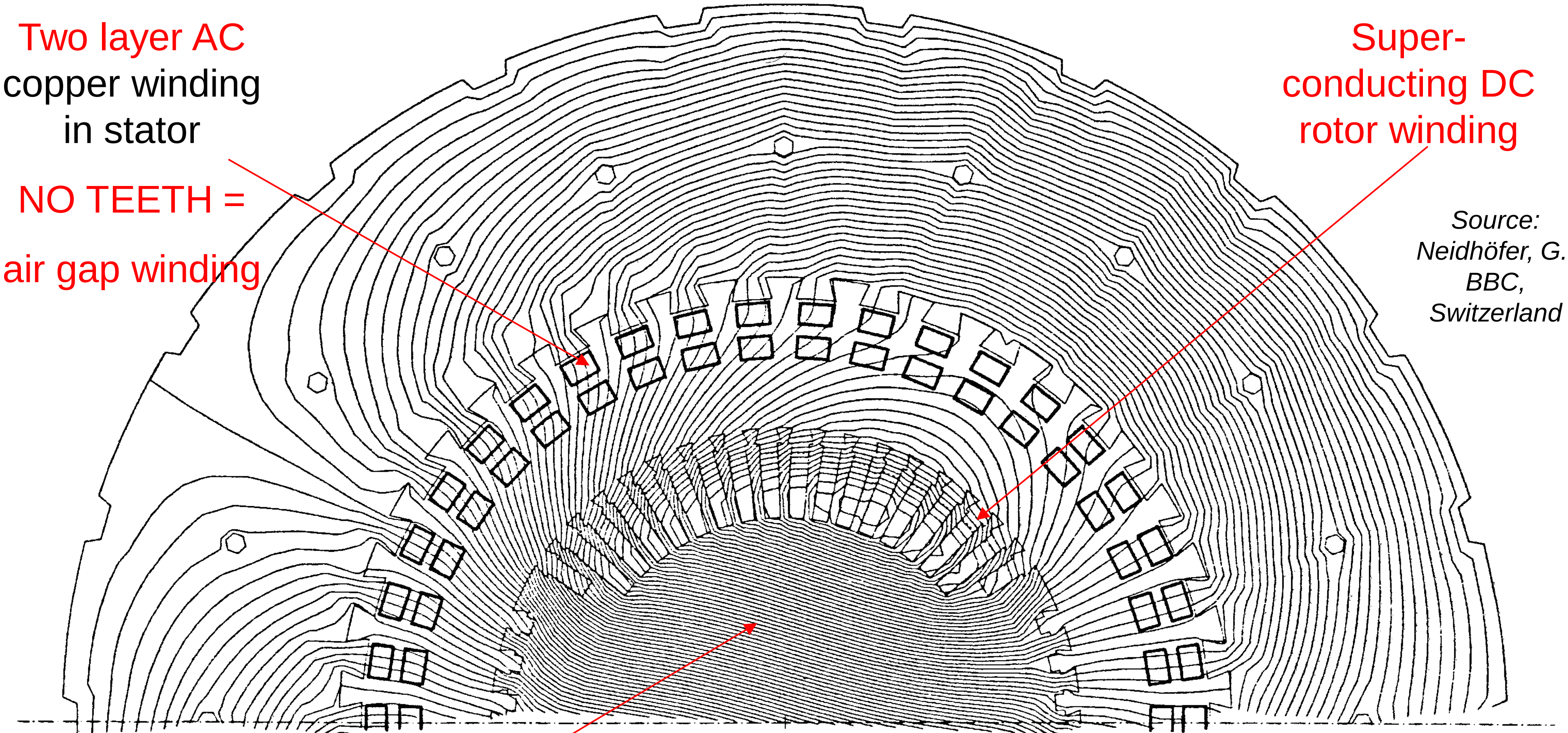
Hence current loading *A* is increased by factor 2.

- **Increase of utilization:** $C_{sc}/C_{norm} = (A_{sc}/A_{norm})\cdot(B_{sc}/B_{norm}) = 2\cdot 1.5 = 3$

Super-conducting synchronous machine is only 1/3 in size at lower total losses !

3. Eddy current losses in winding systems

Three phase air gap winding for super-conducting generator

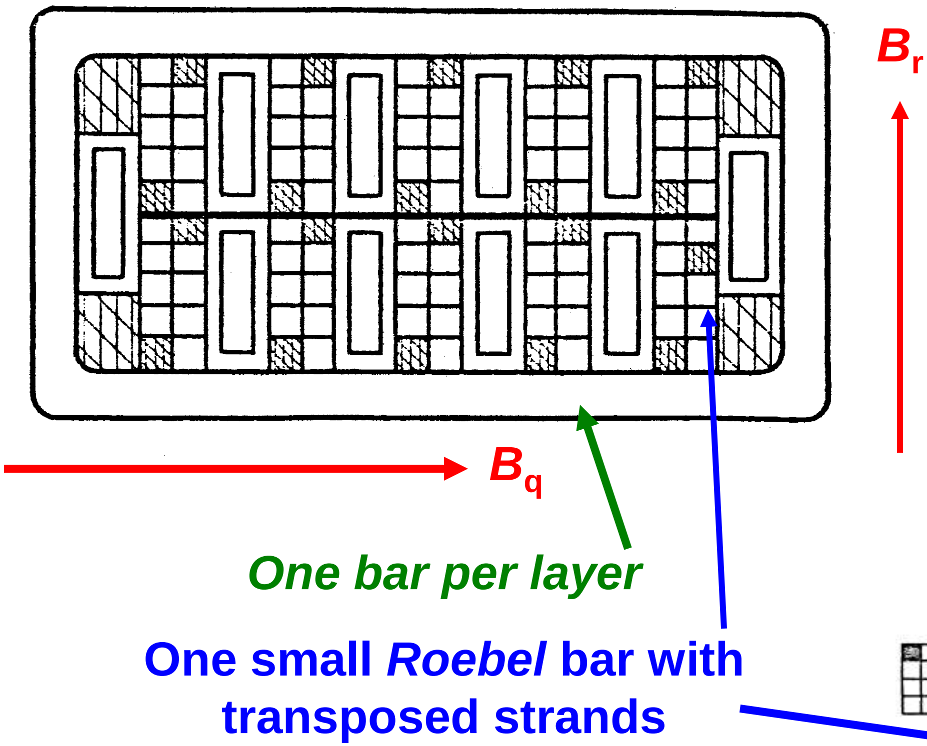


Usually also the rotor iron is made of non-magnetic (stainless) steel due to the high flux density !

3. Eddy current losses in winding systems

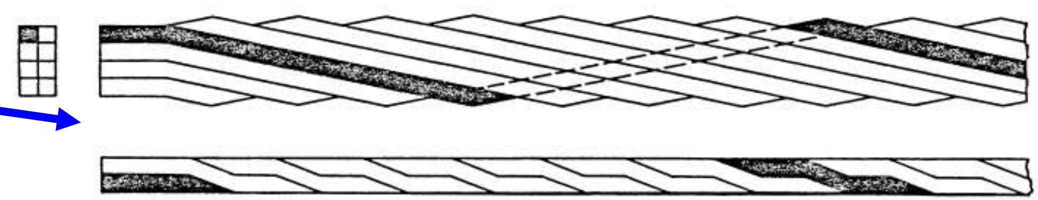
Three phase winding for super-conducting generators

- *Roebel* bars of stator air gap windings are exposed to radial and transversal flux density B_r and B_q due to lack of flux guiding teeth !



- Therefore one bar per layer consist of e.g. 10 twisted and parallel connected small *Roebel* bars, which in their turn consist of e.g. 8 parallel and twisted strands !

- The small *Roebel* bars eliminate mainly the transversal flux linkage, whereas the bar itself eliminated the radial flux linkage !



Source: Neidhöfer, G., BBC, Switzerland

Summary:

Air-gap winding for superconducting machines

- Air-gap winding allows doubling of current loading
- Air-gap winding increases magnetic air-gap strongly, so only super-conducting exciter winding useful for increased rotor Ampere-turns for field excitation
- Air-gap winding is exposed to normal and tangential flux density component
- Double-twisting necessary for coping with tangential and normal AC flux
- Very expensive winding system